

1     **Phosphorus immobilization in Al–drinking water treatment**  
2     **sludge (Al–DWTS) and soil under laboratory conditions**

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4                                   W.C. LI AND Y.Q. ZHAO\*

5     *Centre for Water Resources Research, School of Architecture, Landscape and Civil Engineering,*  
6                                   *University College Dublin, Newstead, Belfield, Dublin 4, Ireland*

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9  
10    **\* Corresponding Author:**

11  
12    Name: Y.Q. Zhao

13    E-mail: yaqian.zhao@ucd.ie

14    Phone: +353-1-7163215

15    Fax: +353-1-7163297

16    Address: Centre for Water Resources Research, School of Architecture, Landscape and Civil  
17                                   Engineering, University College Dublin, Belfield, Dublin 4, Ireland

29 **Abstract:** This study assessed the potential reuse of an aluminium coagulated drinking-water  
30 treatment sludge (Al-DWTS) as a main substrate in constructed wetland to replace soil for the  
31 treatment of P-enriched wastewater. The adsorption isotherm and kinetics of phosphorus (P) removal  
32 from high-P solution by Al-DWTS and a local soil from Bailieborough, Ireland, were studied and  
33 compared under laboratory conditions. Data of P adsorption were well fitted to the Langmuir and the  
34 Freundlich isotherms but the Freundlich isotherm had a higher correlation coefficient. The maximum  
35 P adsorption capacity of the Al-DWTS and the soil was  $39.4 \text{ mg P mg}^{-1}$  and  $9.5 \text{ mg P mg}^{-1}$ ,  
36 respectively, at conditions of pH of 4.0 and temperature of  $23 \text{ }^{\circ}\text{C}$ . Kinetics studies show that  
37 adsorption in both cases followed pseudo-second-order kinetics. The fact that the Al-DWTS  
38 exhibited a significantly higher P adsorption capacity at high-P solution compared with the soil  
39 suggests that Al-DWTS can be a “novel-waste” bioadsorbent with promising application in  
40 wastewater treatment engineering, such as constructed wetland systems.

41

42 **Keywords:** adsorption, alum-drinking water treatment sludge; phosphorus; soil; wastewater  
43 treatment

44

## 45 **1. Introduction**

46 In recent years, much attention has been paid to phosphorus (P) pollution, its causes, ecological  
47 effects and the costs of clean up. Phosphorus enters the natural waters from various industries,  
48 domestic sewage, laundries, running water over phosphate rocks and extensive application of  
49 manure and fertilizers in agriculture. Typically, domestic wastewater has a total P concentration of

50 approximately 10 mg P L<sup>-1</sup>. The principal forms of phosphate are orthophosphate (5 mg P L<sup>-1</sup>),  
51 pyrophosphate (1 mg P L<sup>-1</sup>), and tripolyphosphate (3 mg P L<sup>-1</sup>), together with smaller amounts of  
52 organic phosphate [1]. It is now necessary to adopt effective methods for the removal of P from  
53 wastewater before discharge, in order to meet the effluent limits of 0.5–1.0 mg P L<sup>-1</sup> [2]. Reducing P  
54 levels in wastewater may be achieved by various techniques, such as enhanced biological P removal;  
55 traditional chemical precipitation with aluminium, calcium and iron salts and various  
56 physicochemical methods including reverse osmosis, electrodialysis, contact filtration and  
57 adsorption, etc. [3]. In recent decades, many researchers have investigated removal of phosphate  
58 from wastewater using adsorption techniques with various adsorbents and bioadsorbents such as  
59 activated aluminium oxide, half-burnt dolomite, soil, tamarind nut shell activated carbon [4], fly  
60 ash [5, 6], iron oxide tailings [7], blast furnace slag [8], recycled Fe(III)/Cr(III) hydroxide [9].

61 Drinking-water treatment sludge (DWTS), is a resultant byproduct generated in the process  
62 of using aluminium- or iron-based salts as coagulants during the production of drinking water.  
63 DWTS mainly consists of suspended solids (in terms of turbidity), silt particles, organic matter  
64 (in terms of colour) and microorganisms from source water, together with residual chemicals  
65 (coagulants, polyelectrolytes and conditioning agents) that are added during the treatment  
66 processes. DWTS is classified as high plasticity organic clay. In most cases worldwide,  
67 DWTS is disposed of as waste to landfill. Nevertheless, the application of DWTS in P  
68 immobilization has been increasingly studied to convert it from a “waste” into low cost  
69 bioadsorbents for beneficial reuse. It is now clear that DWTS can be used as a soil amendment to  
70 increase considerably the P sorption capacity of soil for reducing offsite P transport [10–12].  
71 Research has demonstrated that a P-binding capacity of approximately 12.5 g P kg<sup>-1</sup> DWTS can be

72 achieved [13]. A higher capacity up to 37.0 g P kg<sup>-1</sup> DWTS was reported by Dayton and Basta [14]  
73 in examining 18 DWTSs in the US.

74 Recent study by our group in University College Dublin, Ireland focused on exploiting and  
75 developing novel reuses of DWTS as raw material in civil and environmental engineering. Results  
76 have shown some remarkable potential in DWTS for immobilizing a wide range of P species from  
77 simulated P-enriched wastewater. Considerable amounts of P can be adsorbed onto a relatively low  
78 mass of DWTS [15, 16]. Furthermore, the DWTS has been tested as the first of its kind as main  
79 substrate in a constructed wetland system for treating animal farm wastewater with high P levels [17,  
80 18]. Since the main substrate in constructed wetland is normally soil, sand or gravel [19], the use of  
81 easily and locally available DWTS not only provides a low cost technological solution of improving  
82 P removal, but also an effective DWTS management option for its beneficial reuse.

83 The objective of our research was to evaluate the P sorption capacity of an aluminium-coagulated  
84 DWTS (termed as Al-DWTS) under the condition of using a high-P solution. Emphasis was placed  
85 on the comparative study of P-adsorption behaviour and capacity between the Al-DWTS and a local  
86 soil obtained from Bailieborough, Ireland. The soil has previously been employed as the main  
87 substrate in a full-scale constructed wetland system for an agricultural-industry wastewater  
88 treatment. We investigated the equilibrium and kinetics of adsorption of P onto the Al-DWTS and  
89 the soil. We used the Langmuir and Freundlich models to fit the equilibrium isotherms at different  
90 temperatures. We analysed the kinetics of adsorption using pseudo-first-order, pseudo-second-order  
91 and intra-particle diffusion models.

92

93 **2. Materials and methods**

94 *2.1. Al-DWTS, soil and P solution preparation*

95 The Al-DWTS was the brownish-green residual produced at the Ballymore-Eustace Water  
96 Treatment Plant located in South Dublin, Co. Kildare, Ireland from the treatment of a medium colour,  
97 medium turbidity, raw water that had been sourced from the Dublin and Wicklow mountains (upland  
98 catchments of peat over granite bedrock), and stored in Poulaphouca reservoir, County Wicklow.  
99 Dewatered Al-DWTS samples were collected from the dewatering unit of the plant, which uses  
100 aluminium sulphate as main coagulant with a dose of 42–60 mg L<sup>-1</sup> for flocculation. The soil  
101 samples were obtained from the top 10 cm soil of the agricultural land at Lakeland Dairies,  
102 Bailieborough, County Cavan, Ireland, where the same soil has been used for constructing a  
103 full-scale constructed wetland system treating a cheese industry effluent. The Al-DWTS and soil  
104 were air-dried, ground and sieved through a 150 µm sieve size. The major element components of  
105 the Al-DWTS and soil were determined mainly by ICP-analysis and listed in Table 1. This shows  
106 that the Al-DWTS contains an abundant amount of Al (24,880 mg kg<sup>-1</sup> DM (dry mass)) with  
107 significant level of organics indicated by the loss of ignition, which ranged 49–57%. This may be  
108 attributed to humic substances contained in the treated source water. Relatively, the soil contains  
109 much less Al (5,409 mg kg<sup>-1</sup> DM) and high P (2,400 mg kg<sup>-1</sup> DM), S (4,759 mg kg<sup>-1</sup> DM) and Mg  
110 (3,696 mg kg<sup>-1</sup> DM). This may be due to the Irish peat land nature. The stock solution of P was  
111 prepared in distilled water using potassium dihydrogen phosphate (KH<sub>2</sub>PO<sub>4</sub>). All working solutions  
112 were prepared by diluting the stock solution with distilled water.

113 *2.2. Procedures and analysis*

114 P-sorption experiments were conducted by equilibrating 3 g each of Al-DWTS and soil with 30  
115 mL of varying P concentration in 150 mL plastic bottles. The bottles were then placed on a Stuart  
116 Orbital Shaker (SSL 1, Bibby Sterilin Ltd) and the mixture was agitated at 200 rpm for 6 h to ensure  
117 equilibrium. The pH values of the suspensions were adjusted to 3.0, 4.0, 5.5, 7.0, and 9.0 using  
118 either HNO<sub>3</sub> or NaOH. After equilibration, samples were filtered using a 0.45 Millipore membrane  
119 filter to separate the solids from the liquid and the residual P concentration was measured according  
120 to method 8114 (HACH) using a HACH DR/2400 spectrophotometer [16]. For the isotherm studies,  
121 six levels of initial phosphate concentrations (69; 343; 856; 1,142; 1,712; 3,425 mg P L<sup>-1</sup>) were used  
122 while the pH was maintained at an adjusted value of 4.0. Kinetic studies were also carried out at pH  
123 4.0 using 3 g of the adsorbent and six different initial concentrations. The effect of temperature on  
124 adsorption equilibrium was investigated by conducting the shaking experiment in an oven with  
125 temperature varying from 23 to 37 °C.

126

127 **3. Results**

128 *3.1. Effect of contact time and concentration*

129 In order to establish equilibrium time for maximum adsorption and also investigate the kinetics of  
130 the adsorption process, the adsorption of P on the Al-DWTS and the soil at various initial  
131 concentrations was studied as a function of contact time. Figs 1 and 2 show the results. Figure 1  
132 shows that the equilibrium time for the adsorption of phosphate by Al-DWTS was 2 h when the P  
133 concentration ( $C_0$ ) ranged from 69 to 1,712 mg P L<sup>-1</sup>, while for an initial concentration of 3,425 P

134  $\text{mg L}^{-1}$ , the equilibration time was 6 h. Figure 2 indicates that the equilibrium adsorption by soil can  
135 be attained in 2 h when the initial P concentrations are below  $1,142 \text{ mg P L}^{-1}$ . Accordingly, 4 h is  
136 required to reach the equilibrium adsorption when the initial P concentrations are  $1,712 \text{ mg P L}^{-1}$  and  
137  $3,425 \text{ mg P L}^{-1}$ , as shown in Fig. 2. Both the figures exhibit a rapid adsorption trend at the instant of  
138 contact. For instance, 50% adsorption on Al-DWTS was completed within 0.5 h for  $3,425 \text{ mg P L}^{-1}$   
139 and within less than 0.25 h for the soil. Table 2 shows the effect of different initial concentrations on  
140 P adsorption ability by Al-DWTS and soil. The amount of P absorbed per unit mass ( $q_t$ ) of  
141 Al-DWTS and soil seems to increase with an increased  $C_0$ , whereas an exception was observed at P  
142 initial concentration of  $3,425 \text{ mg L}^{-1}$  for soil adsorption.

### 143 3.2. Effect of pH

144 Figure 3 presents the effect of pH on the P adsorption by Al-DWTS and soil. Figure 3 shows that  
145 the optimum pH for both Al-DWTS and soil is 4.0. This corresponds to adsorption capacities of  $31.6$   
146  $\text{mg P g}^{-1}$  and  $8.2 \text{ mg P g}^{-1}$  for Al-DWTS and soil, respectively. Adsorption at pH 9.0 was the least,  
147 with a corresponding adsorption capacity of  $14.7 \text{ mg P g}^{-1}$  and  $2.9 \text{ mg P g}^{-1}$  for Al-DWTS and soil,  
148 respectively. The results indicate that the P adsorption onto Al-DWTS and soil is a physicochemical  
149 process and the adsorption ability is strongly dependent upon solution pH. The adsorptions are  
150 favoured in the acidic range with adsorption maxima obtained at pH 4.0 for both Al-DWTS and soil.

### 151 3.3. Kinetics study

152 The kinetics of P adsorption onto Al-DWTS and soil were studied using two models: pseudo-first-  
153 and second-order kinetics.

154 3.3.1. Pseudo-first-order model

155 The pseudo-first-order equation is given as:

156 
$$\frac{dq_t}{dt} = k_1(q_e - q_t) \quad (1)$$

157 where  $q_t$  is the amount of adsorbate adsorbed at time  $t$  ( $\text{mg g}^{-1}$ ),  $q_e$  the adsorption capacity at  
158 equilibrium ( $\text{mg g}^{-1}$ ),  $k_1$  the pseudo-first-order rate constant ( $\text{h}^{-1}$ ) and  $t$  the contact time ( $\text{h}$ ). The  
159 integration of Eq. (1) with the initial condition,  $q_t = 0$  at  $t = 0$  leads to:

160 
$$\log(q_e - q_t) = \log q_e - \frac{k_1}{2.303}t \quad (2)$$

161 The values of the adsorption rate constant ( $k_1$ ) for P were determined from the plot of  
162  $\log(q_e - q_t)$  against  $t$ .

163

164 3.3.2. Pseudo-second-order model

165 The pseudo-second-order model is described as below [20]:

166 
$$\frac{dq_t}{dt} = k_s(q_e - q_t)^2 \quad (3)$$

167 After integration by applying the boundary conditions, Eq. (3) becomes:

168 
$$q_t = \frac{tk_s q_e^2}{1 + tk_s q_e} \quad (4)$$

169 The initial sorption rate,  $r$  ( $\text{mg/g h}$ ), at  $t \rightarrow 0$  is defined as

170 
$$r = k_s q_e^2 \quad (5)$$

171 Eq. (4) can then be rearranged to obtain

172 
$$q_t = \frac{t}{1/r + (1/q_e)t} \quad (6)$$

173 Thus  $q_e$  can be obtained from the slope of  $t/q_t$  versus  $t$  and  $r$  is obtained from the intercept. Therefore,  
 174  $k_s$  can be calculated from Eq. (5). Figures 4 and 5 show the plot of Eq. (6) for adsorption of P onto  
 175 Al-DWTS and soil, respectively. The results demonstrate a linear relationship between adsorbed  
 176 phosphate and  $t$ , with high correlation coefficients. The kinetic parameters for the pseudo-first- and  
 177 second-order equations and correlation coefficients are tabulated in Table 3 (for Al-DWTS) and  
 178 Table 4 (for soil). By inspecting  $R^2$  in Tables 3 and 4, it is clear that the pseudo-second-order model  
 179 is better than the pseudo-first-order model to describe the P adsorption for both Al-DWTS and soil.  
 180 Several authors have also reported the validity of the pseudo-second-order model in description of P  
 181 adsorption onto ZnCl<sub>2</sub> activated coir pith carbon [3] and recycled Fe(III)/Cr(III) hydroxide [9] as  
 182 well as alunite [21].

183 Plots of  $q_e$  and  $r$  against  $C_0$  were regressed to obtain the values in terms of  $C_0$  with a high  
 184 regression coefficient for Al-DWTS ( $R^2 = 0.999, 0.996$ , respectively). Regressions were gained to  
 185 the best fitting of  $q_e$  and  $r$  against  $C_0$  for soil with a slightly lower regression coefficient ( $R^2 = 0.960$ ,  
 186  $0.976$ , respectively). Nevertheless,  $q_e$  and  $r$  can be expressed as a function of  $C_0$ , as shown in Eq. (7)  
 187 and Eq. (8) for Al-DWTS, and Eq. (9) and Eq. (10) for soil, respectively.

$$188 \quad q_e = 0.0092 \times C_0 + 0.3784 \quad (7)$$

$$189 \quad r = -2 \times 10^{-5} \times C_0^2 + 0.1112 \times C_0 - 2.4243 \quad (8)$$

$$190 \quad q_e = 0.0273 \times C_0^{0.7264} \quad (9)$$

$$191 \quad r = -1 \times 10^{-6} \times C_0^2 + 0.0188 \times C_0 + 1.9256 \quad (10)$$

192 Substituting the values of  $q_e$  and  $r$  into Eq. (6), the relationship of  $q_t$ ,  $C_0$  and  $t$  can be  
 193 represented for Al-DWTS (Eq. (11)) and soil (Eq. (12)) as follows:

$$194 \quad q_t = \frac{t}{1/(-2 \times 10^{-5} \times C_0^2 + 0.1112 \times C_0 - 2.4243) + (1/(0.0092 \times C_0 + 0.3784)) \times t} \quad (11)$$

195

$$q_t = \frac{t}{1/(-1 \times 10^{-6} \times C_0^2 + 0.0188 \times C_0 + 1.9256) + (1/(0.0273 \times C_0^{0.7264})) \times t} \quad (12)$$

197 These equations can then be used to derive the amount of P adsorbed on Al-DWTS and soil at any  
198 given  $C_0$  (from 69 to 3,425 mg P L<sup>-1</sup>) and  $t$ .

199

### 200 3.4. Adsorption isotherm

201 To assess the adsorption potential of Al-DWTS and soil for high-P solution, Langmuir and  
202 Freundlich isotherms were used for fitting sorption equilibrium data. Equations (13) and (14)  
203 respectively give the linear forms of the Langmuir isotherm and the Freundlich isotherm.

$$\frac{C_e}{q_e} = \frac{1}{Q_0 b} + \frac{C_e}{Q_0} \quad (13)$$

$$\log q_e = \log k_d + (1/n) \log C_e \quad (14)$$

206 where  $q_e$  is defined as before (mg P g<sup>-1</sup>),  $b$  (L mg<sup>-1</sup>) a sorption constant related to P binding energy,  
207  $Q_0$  the maximum adsorption capacity (mg P g<sup>-1</sup> sludge) and  $C_e$  is the equilibrium P concentration  
208 (mg P L<sup>-1</sup>). The slope and the intercept of the plot of  $(C_e/q_e)$  versus  $C_e$  gives the values of  $Q_0$  and  $b$ .  
209  $k_d$  is the distribution coefficient, and  $n$  is a parameter of the Freundlich model.

210 By fitting the equilibrium data at 23, 30 and 37 °C with Eq. (13) and Eq. (14), respectively, the  
211 isotherms for Al-DWTS and soil are generated. Figures 6 and 7 illustrate this. Table 5 lists the  
212 theoretical parameters of isotherms along with correlation coefficients. It is seen that the  
213 experimental data of P adsorption onto the Al-DWTS and the soil could be well fitted by the two  
214 models. The Freundlich isotherm exhibited a better fitting than Langmuir isotherm, and this is in  
215 agreement with that reported recently by Mortula and Gagnon [22] in a similar study. In addition,

216 Table 5 also shows that the adsorption capacity increased from 39.4 to 42.9 mg P g<sup>-1</sup> for Al-DWTS  
217 and from 9.49 to 11.03 mg P g<sup>-1</sup> for soil when the temperature was increased from 23 to 37 °C.

218

#### 219 **4. Discussion**

220 The aim of this study was to provide comparative data on P adsorption by Al-DWTS and a local  
221 soil. A series of adsorption experiments were designed and in particular, from the results, the  
222 Al-DWTS was found to be capable of removing P even at a very high P level. Table 5 shows that the  
223 P adsorption capacity of Al-DWTS (39.4 mg P g<sup>-1</sup>) is more than four times greater than that of soil  
224 (9.5 mg P g<sup>-1</sup>). Although various factors can contribute to P retention mechanisms in the Al-DWTS  
225 and soil, it is believed that aluminium oxide is the major cause because it is particularly strong in  
226 binding P through ligand exchange and precipitation reactions, which have been investigated  
227 previously [23, 24]. Table 1 shows that Al in Al-DWTS is eight-fold greater than that in soil.  
228 Although the properties of Al-DWTS are variable and dependent upon the characteristics of the raw  
229 waters and the coagulant used, which is believed to result in different P adsorption capacities, it is  
230 reasonable to conclude that the alum based DWTS has a very high P adsorption capacity over soil  
231 due to the feature of significantly high Al content. As such, the feasibility of augmenting soil's P  
232 sorption capacity by mixing DWTS into soils as a new chemical-based P immobilization method has  
233 already been investigated and confirmed by different researchers [10–12, 25]. In addition, the  
234 specific surface area (SSA) of the Al-DWTS tested was in the range of 49.0–62.3 m<sup>2</sup> g<sup>-1</sup> [26].  
235 Although the SSA of the soil was not monitored, in comparison to the range of SSA of other  
236 materials reported in literature such as 2.6–3.9 m<sup>2</sup> g<sup>-1</sup> [27] and 6.8–31.4 m<sup>2</sup> g<sup>-1</sup> [28], the Al-DWTS

237 used herein can be seen to have a comparatively higher SSA. This is believed to be relevant to the  
238 high P adsorption capacity.

239 With regard to the factors that affect the P adsorption behaviour on Al-DWTS and soil, initial  
240 concentrations, contact time, pH and temperature have all shown pronounced effects on the  
241 adsorption capacity of both adsorbents (see Figs 1–3, Tables 2, 5). In particular, computed models  
242 (Eq. (11) and (12)) derived from the data of this study have provided a quantitative description of the  
243 integrated effect of some major factors especially the initial P concentration on adsorption behaviour.  
244 Although P adsorption is a complicated process, ligand exchange may be the dominating mechanism  
245 [23]; more Al content in Al-DWTS may provide more activated exchange sites than soil. From Figs  
246 1 and 2, it seems that when P adsorptions on Al-DWTS and soil occur at lower concentration, the  
247 time required to achieve a definite fraction of equilibrium is independent of initial concentration. It is  
248 reasonable to expect that at lower concentration, the ratio of the initial number of P molecules to the  
249 available exchange sites is low and subsequently the fractional adsorption becomes independent of  
250 initial concentration. But, at a higher concentration, fewer exchange sites are available to occupy, so  
251 the amount of P adsorbed is dependent upon the initial concentration. In a previous study [15], P  
252 adsorption capacity of  $10.2 \text{ mg PO}_4^{3-} \text{ g}^{-1}$  Al-DWTS was obtained at a low P concentration which  
253 simulated the typical P level in municipal wastewater. This reflects the effect of initial P  
254 concentration on adsorption capacity.

255 The amount of P absorbed onto Al-DWTS and soil increased with an increase of agitation time  
256 before equilibrium was reached (Figs 1 and 2). P was initially adsorbed by the activated exchange  
257 sites in the exterior surface. When the adsorption at the exterior surface reached the saturation level,  
258 P begins to diffuse into the pores within the particles. The determination of pore size distribution of

259 the Al-DWTS indicated that pores with sizes less than 5.98 nm contributed 50% of the surface area  
260 while pores of size less than 9.67 nm contributed 90% of the surface area. The pore size larger than  
261 20 nm only contributed an insignificant amount to the surface area [26]. Through the intra-particle  
262 diffusion study [29, 30], an intra-particle diffusion coefficient  $k_{id}$  is given by the equation:

$$263 \quad q_t = k_{id} t^{1/2} \quad (15)$$

264 Figures 8 and 9 show the plots of  $q_t$  versus  $t^{1/2}$  for Al-DWTS and soil, respectively. Table 6 lists the  
265 calculated intra-particle diffusion coefficient  $k_{id}$  values. Figures 8 and 9 reveal two separate regions  
266 active in the P adsorption process on Al-DWTS and soil at high initial concentration. The initial  
267 portion is attributed to the mass transfer of P molecules from bulk solution to absorbent surface; the  
268 second portion is the intra-particle diffusion on the absorbent. It is believed that the intra-particle  
269 diffusion might be the rate-controlling step in the P adsorption process. As mentioned previously, the  
270 pH of the aqueous solution is an important variable that influences the P adsorption on Al-DWTS  
271 and soil. As Fig. 3 shows, the amount of P adsorbed onto Al-DWTS and soil tends to decrease when  
272 pH increases from 4.0 to 9.0. In an early study [23], the increase of  $\text{OH}^-$  in solution could affect  
273 the electrostatic properties of the sludge, which makes the surface charge of the Al-DWTS change  
274 from positive to negative. This is confirmed by measuring the zeta potential, which ranged from  
275 +75.8 to -33.7 mV corresponding to a pH change from 4.3 to 9.0. The more negatively charged  
276 surface would repulse the negatively charged species (such as  $\text{PO}_4^{3-}$ ) in solution to break the  
277 P-binding process.

278 Although chemical precipitation of the various forms of calcium phosphates is favoured at a pH  
279 above 7.5 [31], this is not the case for the Al-DWTS and soil studied in spite of the reasonably high  
280 contents of calcium in Al-DWTS and soil (see Table 1). It is noted in Fig. 3 that when  $\text{pH} < 4.0$ ,

281 such as pH = 3.0, the P adsorption capacity of Al-DWTS and soil decreases. This may be caused by  
282 a higher solubility of aluminium oxide as it occurs below a pH value of about 4.0–4.5 [8, 32]. The  
283 effect of temperature on the P adsorption capacity of Al-DWTS and Bailieborough soil shows (in  
284 Table 5) that the sorption of phosphate is an endothermic process. Yet, although the P adsorption on  
285 Al-DWTS tends to increase with increased temperature from 23 °C to 37 °C, there is a relatively  
286 slight increase on soil. The sorption constant  $b$ , which relates to the P binding energy, increased from  
287 0.0156 to 0.0190 L mg<sup>-1</sup> for Al-DWTS and increased from 0.0022 to 0.0029 L mg<sup>-1</sup> for soil at  
288 adsorption conducted at temperatures from 23 °C to 37 °C. This suggests that increasing temperature  
289 favours the P sorption.

290

## 291 **5. Conclusions**

292 An aluminium coagulated drinking water treatment sludge (Al-DWTS) and a constructed  
293 wetland soil were assessed for their P removing ability. The same trends of P adsorption were  
294 obtained in both cases. But, the Al-DWTS exhibited a significant P immobilization ability at high-P  
295 concentration in contrast to the soil. P adsorption capacity on Al-DWTS in high-P solution is 39.4  
296 mg P g<sup>-1</sup>, which is more than four times greater than the value (9.14 mg P g<sup>-1</sup>) on soil. Analysis of  
297 kinetic data showed that uptake of P onto Al-DWTS and soil followed pseudo-second-order kinetics.  
298 Equilibrium adsorption data of Al-DWTS and soil obey both Langmuir and Freundlich isotherms  
299 with the Freundlich isotherm being better than the Langmuir. Maximum P removal occurred at pH =  
300 4.0 for both adsorbents tested. The sorption capacity of both Al-DWTS and soil increases at a  
301 temperature range from 23 to 37 °C. Overall, this result provides the technical support for using

302 Al-DWTS to benefit soil as an absorbent for removal of P in a wider range of concentration from  
303 P-rich wastewaters.

304

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394 **Tables:**

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Table 1 Principal chemical compositions of Al-DWTS and soil (\*DM denotes dry mass)

Chemical composition	Unit	Amount	
		Al-DWTS	Soil
Aluminium (Al)	mg kg-DM <sup>-1*</sup>	42,880.0	5,409.0
Iron (Fe)	mg kg-DM <sup>-1</sup>	2,465.0	2,231.0
Calcium (Ca)	mg kg-DM <sup>-1</sup>	1,964.0	3,400.0
Magnesium (Mg)	mg kg-DM <sup>-1</sup>	227.4	3,696.0
Lead (Pb)	mg kg-DM <sup>-1</sup>	4.8	5.3
Arsenic (As)	mg kg-DM <sup>-1</sup>	23.6	1.4
Mercury (Hg)	mg kg-DM <sup>-1</sup>	N/A	< 0.4
Sulphur (S)	mg kg-DM <sup>-1</sup>	18.9	4,759.0
Chlorine (Cl)	mg kg-DM <sup>-1</sup>	16.0	11.7
Phosphorus (P)	mg kg-DM <sup>-1</sup>	154	2,400.0
Moisture content	%	25.5	15.5
Loss in dry mass on ignition	%	49–57	N/A

Table 2 P adsorption capacity of Al-DWTS and soil at different initial concentrations ( $T = 23\text{ }^{\circ}\text{C}$ ,  $\text{pH} = 4.0$ )

Initial concentration (mg P L <sup>-1</sup> )	P adsorption capacity, $q_e$ (mg P g <sup>-1</sup> )	
	Al-DWTS	Soil
69	0.67	0.52
343	3.32	2.28
856	8.37	3.67
1,142	11.08	4.56
1,712	16.60	8.35
3,425	31.64	8.15

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Table 3 Kinetic parameters for the removal of P by Al-DWTS ( $T = 23\text{ }^{\circ}\text{C}$ ,  $\text{pH} = 4.0$ )

$C_0$ (mg P L <sup>-1</sup> )	First-order model		Second-order model		
	$k_1$ (h <sup>-1</sup> )	$R^2$	$r$ (mg g <sup>-1</sup> h <sup>-1</sup> )	$k_s$ (g mg <sup>-1</sup> h <sup>-1</sup> )	$R^2$
69	1.58	0.970	6	13.37	0.995
343	1.38	0.967	30	2.72	0.999
856	1.14	0.985	75	1.07	0.998
1,142	0.90	0.946	96	0.78	0.998
1,712	0.87	0.967	112	0.41	0.999
3,425	0.72	0.943	86.9	0.09	0.999

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Table 4 Kinetic parameters for the removal of P by soil ( $T = 23\text{ }^{\circ}\text{C}$ ,  $\text{pH} = 4.0$ )

$C_0$ (mg P L <sup>-1</sup> )	First-order model		Second-order model		
	$k_1$ (h <sup>-1</sup> )	$R^2$	$r$ (mg g <sup>-1</sup> h <sup>-1</sup> )	$k_s$ (g mg <sup>-1</sup> h <sup>-1</sup> )	$R^2$
69	2.23	0.990	3.86	14.3	0.995
343	1.59	0.990	7.85	1.51	0.998
856	3.15	0.997	17.8	1.32	0.998
1,142	1.95	0.973	21.7	1.04	0.999
1,712	1.17	0.977	35.6	0.51	0.999
3,425	0.70	0.874	54.4	0.82	0.999

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Table 5 Langmuir and Freundlich isotherms constants obtained at obtained  $\text{pH} = 4.0$ 

Adsorbent	$T$ ( $^{\circ}\text{C}$ )	Langmuir			Freundlich		
		$Q_0$ (mg P g <sup>-1</sup> )	$b$	$R^2$	$k_d$	$1/n$	$R^2$
Al-DWTS	23	39.4	0.0156	0.973	0.994	0.668	0.986
	30	40.7	0.0167	0.962	1.137	0.661	0.989
	37	42.9	0.0190	0.969	1.316	0.655	0.985
Soil	23	9.5	0.00220	0.931	0.125	0.563	0.938
	30	10.1	0.00256	0.942	0.163	0.541	0.945
	37	11.0	0.00293	0.962	0.210	0.514	0.945

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Table 6 Intraparticle diffusion rate coefficient of P adsorption on Al-DWTS and soil ( $T = 23 \text{ }^{\circ}\text{C}$ ,  $\text{pH} = 4.0$ )

$C_0$ ( mg P L <sup>-1</sup> )	Al-DWTS		Soil	
	$k_{id}$	$R^2$	$k_{id}$	$R^2$
69	0.12	0.94	0.10	0.85
343	0.45	0.97	0.56	0.94
856	1.37	0.86	0.65	0.92
1,142	1.71	0.88	0.77	0.92
1,712	1.99	0.91	1.52	0.99
3,425	6.22	0.95	0.98	0.95

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411 **Figure Captions:**

412 **Fig. 1.** Time variation of P-adsorption at various initial P concentrations for Al-DWTS ( $T = 23\text{ }^{\circ}\text{C}$ ,  
413  $\text{pH} = 4.0$ )

414 **Fig. 2.** Time variation of P adsorption at various initial P concentrations for soil ( $T = 23\text{ }^{\circ}\text{C}$ ,  $\text{pH} =$   
415  $4.0$ )

416 **Fig. 3.** Effect of pH on P-adsorption onto Al-DWTS and soil ( $C_0 = 3,425\text{ mg L}^{-1}$ ,  $T = 23\text{ }^{\circ}\text{C}$ )

417 **Fig. 4.** Plot of the pseudo-second-order adsorption kinetics of P on Al-DWTS at different initial  
418 concentrations ( $T = 23\text{ }^{\circ}\text{C}$ ,  $\text{pH} = 4.0$ )

419 **Fig. 5.** Plot of the pseudo-second-order adsorption kinetics of P on soil at different initial  
420 concentrations ( $T = 23\text{ }^{\circ}\text{C}$ ,  $\text{pH} = 4.0$ )

421 **Fig. 6.** Langmuir (upper) and Freundlich (lower) adsorption isotherms of P adsorption onto  
422 Al-DWTS at different temperatures ( $\text{pH} = 4.0$ )

423 **Fig. 7.** Langmuir (upper) and Freundlich (lower) adsorption isotherms of P adsorption onto soil at  
424 different temperatures ( $\text{pH} = 4.0$ )

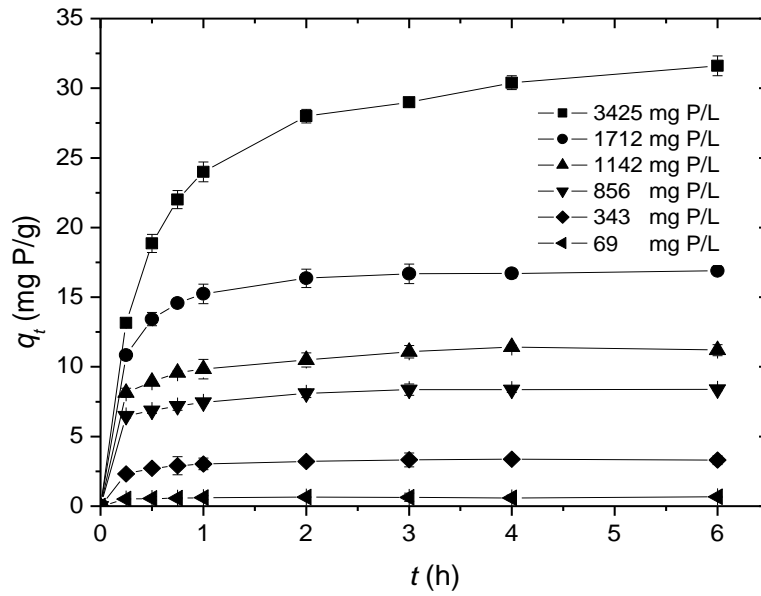
425 **Fig. 8.** Intraparticle diffusion plot for the P adsorption on Al-DWTS ( $T = 23\text{ }^{\circ}\text{C}$ ,  $\text{pH} = 4.0$ )

426 **Fig. 9.** Intraparticle diffusion plot for the P adsorption on soil ( $T = 23\text{ }^{\circ}\text{C}$ ,  $\text{pH} = 4.0$ )

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429 **Figures:**

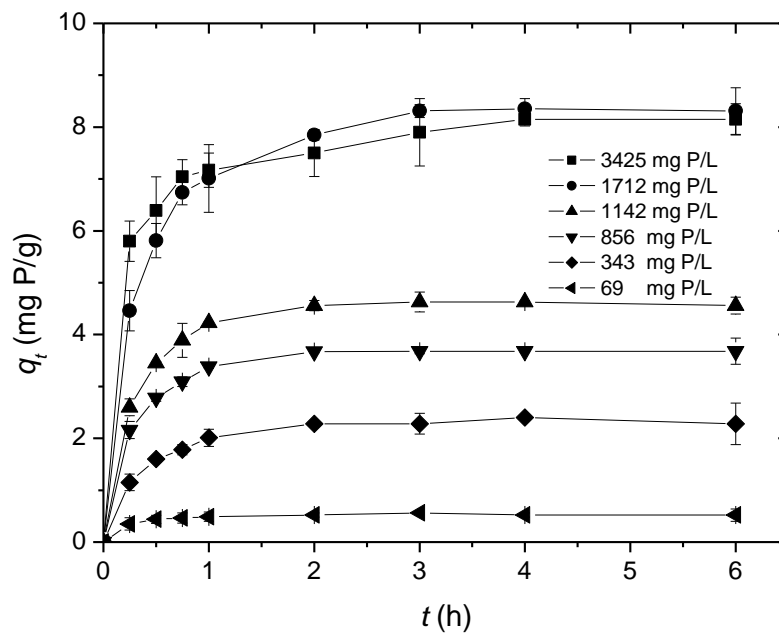


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**Fig. 1.**

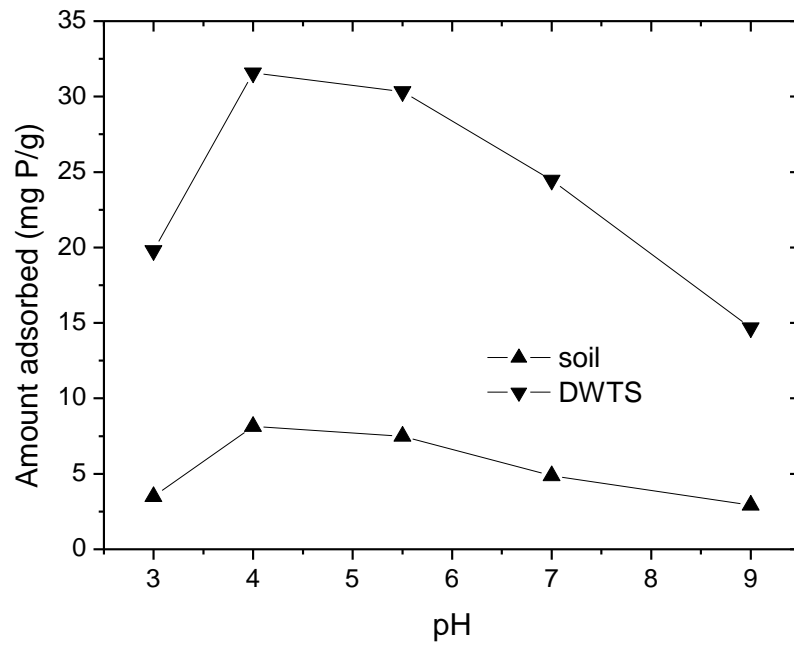


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**Fig. 2.**

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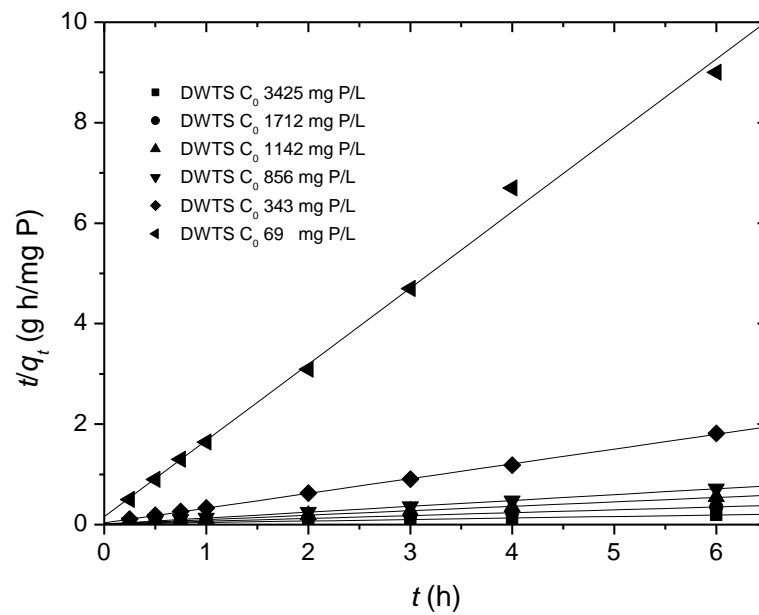
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Fig. 3.

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Fig. 4.

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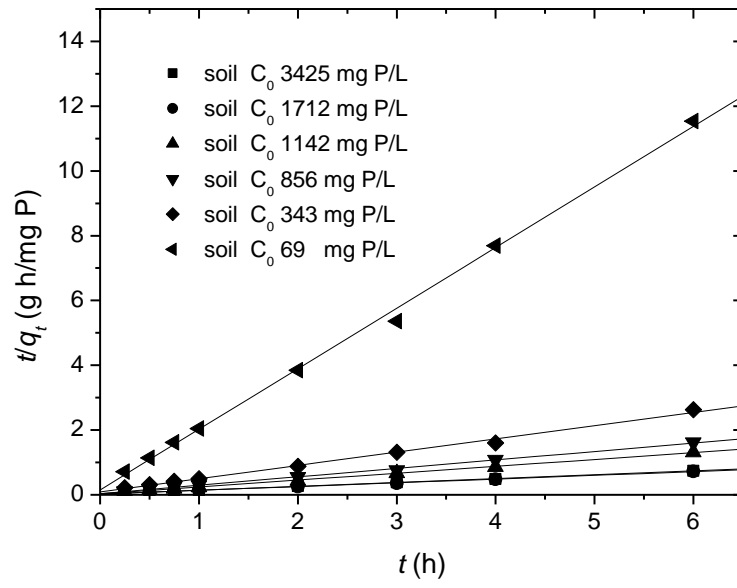


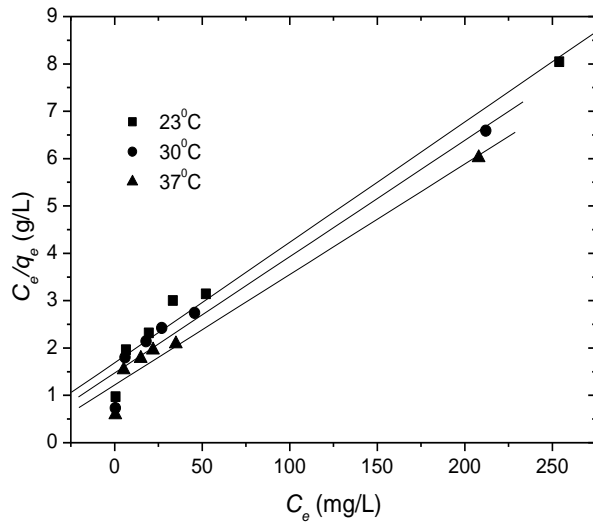
Fig. 5.

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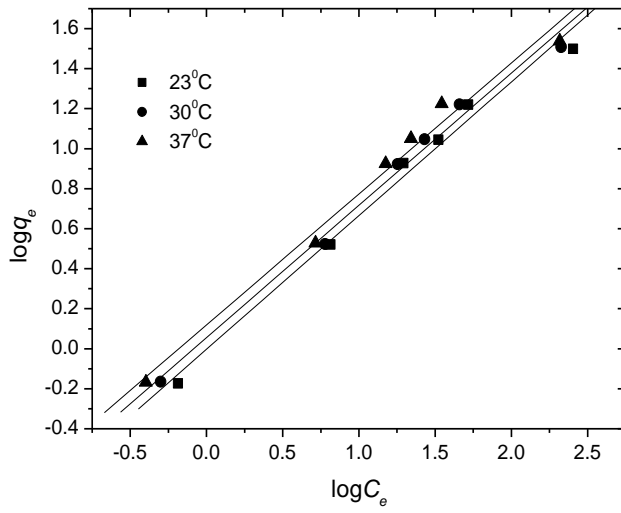
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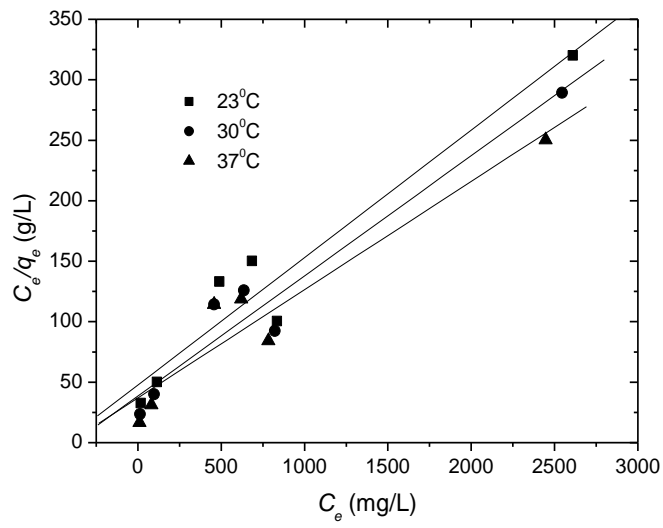
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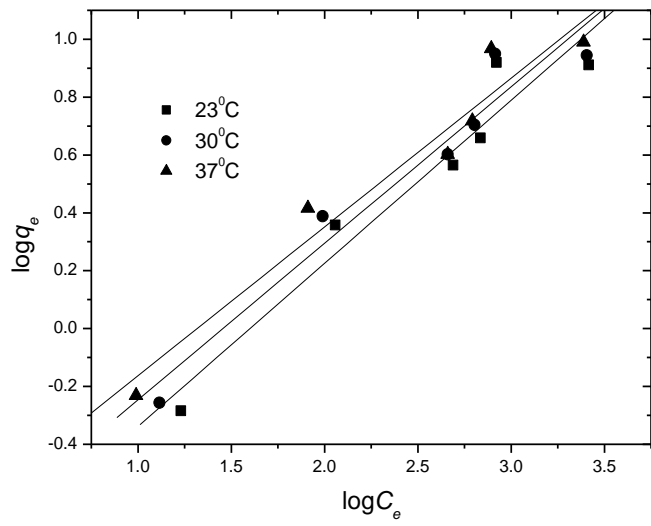
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Fig. 6.

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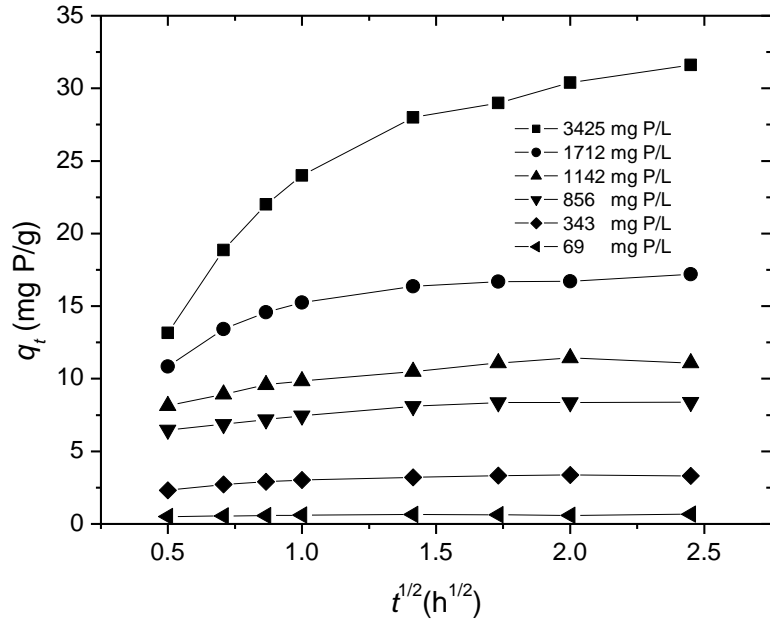
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**Fig. 7.**

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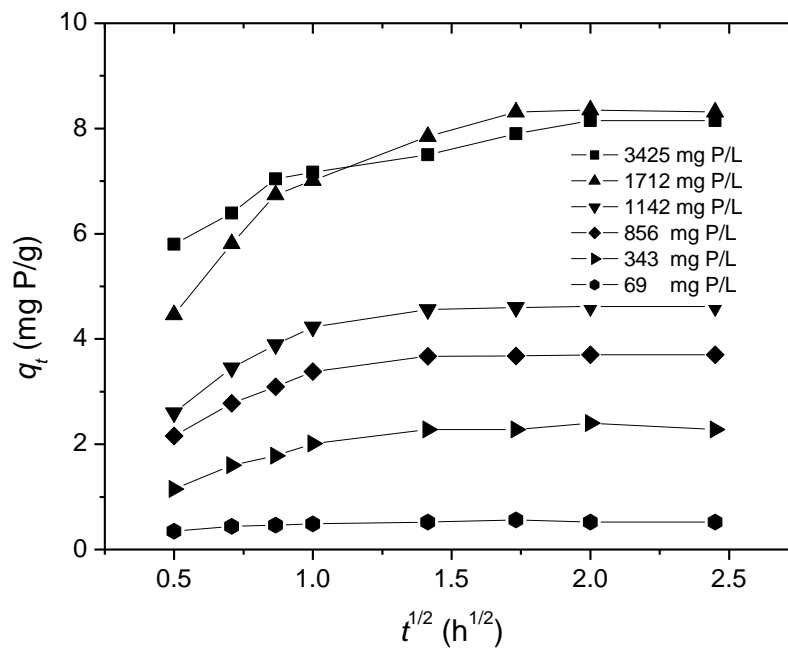


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Fig. 8.



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Fig. 9.