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# 1 Sensor Measurement Strategies for Monitoring 2 Offshore Wind and Wave Energy Devices

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4 and Vikram Pakrashi<sup>1</sup>

## 5 **Abstract**

6 While the potential of offshore wind and wave energy devices is well  
7 established in terms of environmental impact, operations and maintenance  
8 issues are still not very well researched or understood. One of the important  
9 aspects in this regard is the lack of access to these devices since they are  
10 typically situated in high wind and wave conditions to generate more energy.  
11 Consequently, deployment of sensors for such devices is an important issue  
12 since they can measure the response of these devices in an as-deployed  
13 condition and assessments or intervention decisions may be made based on  
14 the fusion of data of such sensors and through the choice of intelligent  
15 markers or modelling. While scaled model testing of devices in ocean basin  
16 has gained popularity and wide acceptance over time, research in the  
17 direction of developing guidelines for sensor measurement or placement  
18 strategies are currently not in place. This paper addresses some specific  
19 aspects of sensor choice, measurement and placement. In this regard, the  
20 performances of the sensors are considered in terms of their receiver  
21 operating characteristics (ROC) and uncertainties related to measurements are  
22 addressed. The option of using multiple, cheaper sensors of seemingly  
23 inferior performance as opposed to the deployment of a small number of

24 expensive and accurate sensors is also explored. Practical aspects of testing  
25 are addressed in terms of exposure conditions and the performance of  
26 different sensors. Tests have been carried out in an ocean wave basin and the  
27 sensor placement for these tests has been used as a case study.

## 28 **1 Introduction**

29 Both offshore wind and wave energy technology has seen major advances in  
30 recent years. Wave energy in particular is growing in popularity (Falcão  
31 2010; Mccullen et al. 2002). Operations and maintenance (O&M) costs are a  
32 highly relevant factor in the overall financial assessment of such projects, all  
33 the more so in offshore projects due to lower availability of the device  
34 (O'Connor et al. 2013). This has pushed the need for reliable structural  
35 monitoring systems for accurate and reliable information about the health of  
36 these energy conversion devices. With a move in recent times towards  
37 offshore energy solutions, loss in ease of accessibility may lead to damage  
38 going undetected, and the increased risk of catastrophic failure (Swartz et al.  
39 2010).

40 There is clear financial benefit to optimizing time between inspections and  
41 scheduled maintenance work, which affects the uptime of systems while also  
42 coming with their own costs- an unscheduled maintenance event is five times  
43 more costly than one that is scheduled (Adams et al. 2011). However, high  
44 costs related to some sensing systems outweigh the benefits to O&M cost  
45 savings so the value of expensive sensing systems must be evaluated.

46 There are many forms of sensing systems, based on various technologies.  
47 Accelerometers have been successfully applied to identifying and locating the  
48 presence of structural damage in offshore structures (Mangal 2001), as well  
49 as motion cameras and load cells (V.JAKSIC; ref; ref) and Fiber Bragg

50 Grating (FBG) to measure strain. Cameras can even be employed in  
51 underwater situations to detect damage (O'Byrne et al. 2014) where marine  
52 growth exasperates fatigue damage. However, little is known of the relative  
53 merits of these technologies.

54 Wireless sensor networks (WSN) are a promising technology which have in  
55 recent years gained much attention from academia and industry alike. The  
56 application of WSN technology to structural health monitoring (SHM) has  
57 the potential to provide a substantial and quantifiable improvement to  
58 existing monitoring solutions for civil infrastructure (Boyle et al. 2011)  
59 .While wired SHM systems would require more maintenance and more  
60 frequent site visits as wires can be damaged over time, wireless SHM systems  
61 offer flexibility, even on difficult to access structures, and significantly  
62 reduced costs of installation and maintenance.

63 However, some of the existing wireless systems for SHM still have high  
64 power consumption. The high power consumption and the limited power  
65 budget make these systems unsuitable for long-term installation on a structure  
66 and requires frequent site visits for system maintenance.

67 WSN nodes are battery powered and because of their limited energy source  
68 they are not suitable for long-term structural health monitoring applications.

69 With the focus on enhancing the life time of a wireless sensor node, a popular  
70 is by complementing an energy harvesting technique with an efficient energy  
71 management algorithm (Sharma et al. 2010). This approach has the potential

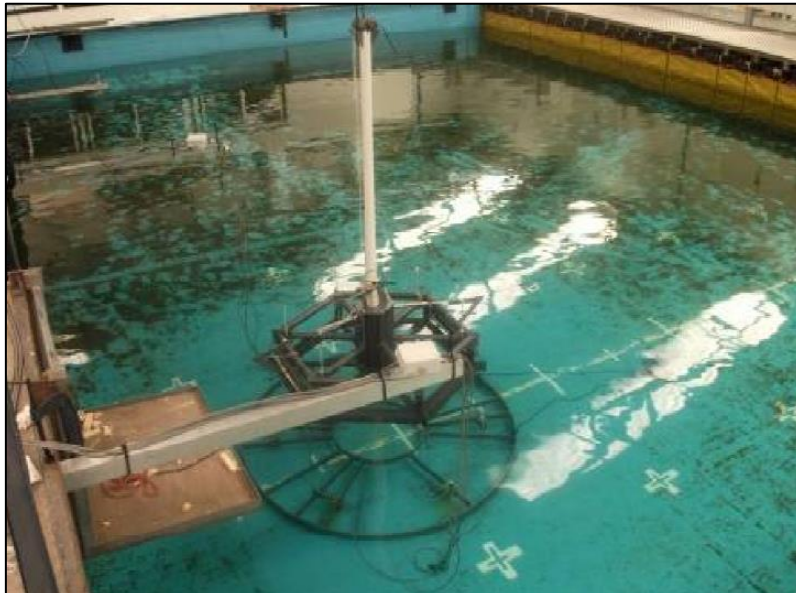
72 to achieve self-sustainability of the node with harvesting energy from the  
73 environment and effectively managing the node activity (i.e. the sampling  
74 rate of the sensors) according to the energy levels and the dynamics of the  
75 phenomenon observed (Srbinovski et al. 2015unpublished)

76

## 77 **2 Experimental Model**

### 78 **2.1 Model**

79 A scaled Tension Leg Platform (TLP), a truss like structure with a hexagonal  
80 base, was tested in this study. This device consists of a gravity base  
81 connected by six mooring tethers to the Buoyancy Ring and the Upper  
82 Structure and the Tower and Nacelle, all as shown in fig 1.



83

84

Figure 1 TLP Model

85

## **2.2 Instrumentation and Testing**

86 The model was instrumented with 6 Tedeo-Huntleigh stainless steel single  
87 ended bending beam load cells which were attached to the six mooring line  
88 cables and bolted to the gravity base. These measured the cable tension in  
89 Newtons (N). The instantaneous positions of 3 reflective markers, which  
90 were attached to the six corners of the hexagonal base, were monitored by 4  
91 Qualisys 3-Series Oqus Marker Tracking Cameras with a sampling frequency  
92 of 32Hz. A Laser Doppler Vibrometer (LDV) was also employed during  
93 testing to record the velocity of the TLP. This high resolution technology  
94 samples at a rate of 480 Hz. Displacements and velocities were recorded in the  
95 wave direction, as this was considered the most critical plane.

96 The model was tested at the Hydraulics and Maritime Research Centre  
97 (HMRC), University College Cork (UCC), Ireland in its Ocean Wave Basin.  
98 A variety of periods and wave amplitudes were used and the Bret Schneider  
99 wave spectrum was chosen, to best represent a true sea state.

100

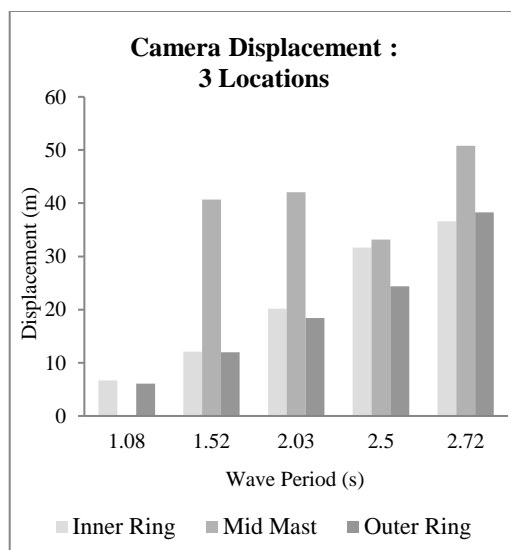
101 **3 Results**

102 **Displacement**

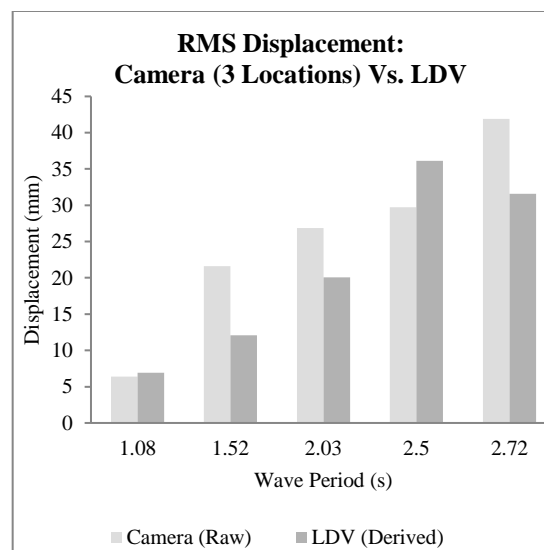
103 The camera recorded the position of the TLP at 3 different locations; the  
104 Inner Ring, the Outer Ring and the Middle Mast. The velocity of the structure  
105 as recorded by the LDV was used to find displacement values.

106 Figure 2(a) shows the displacements recorded by the camera at the 3 tracked  
107 positions. Due to the far larger amplitude of displacement at the mid mast  
108 position, due to the flexible nature of the mast and its sensitivity, these  
109 readings were omitted from the average value shown in figure 2 (c), as they  
110 were viewed to be skewing the data (see figure 2 (b) ).

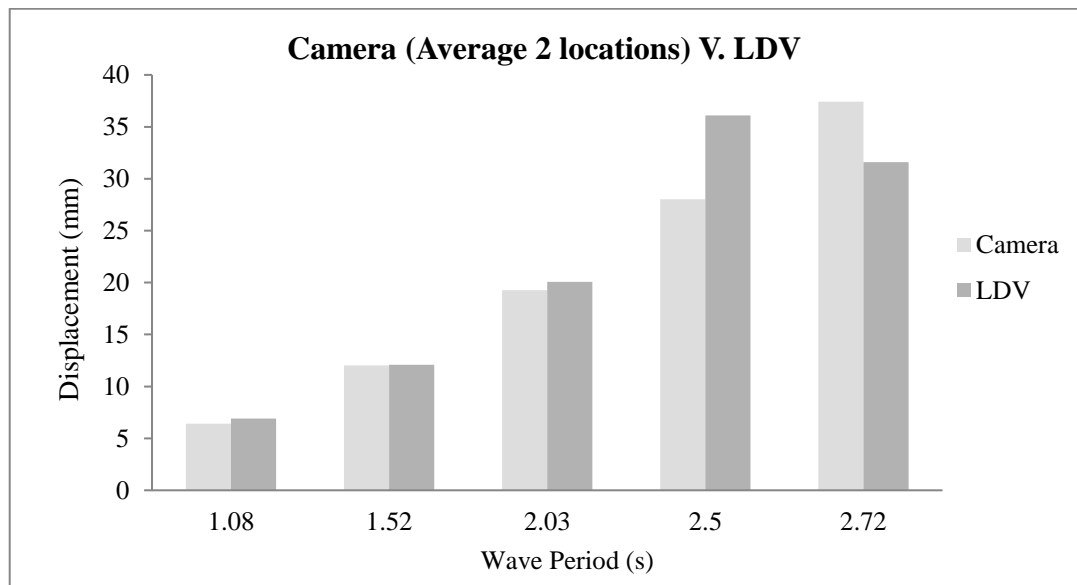
111



**2(a)**



**2(b)**



2(c)

112 **Figure 2 Displacement**

113

114

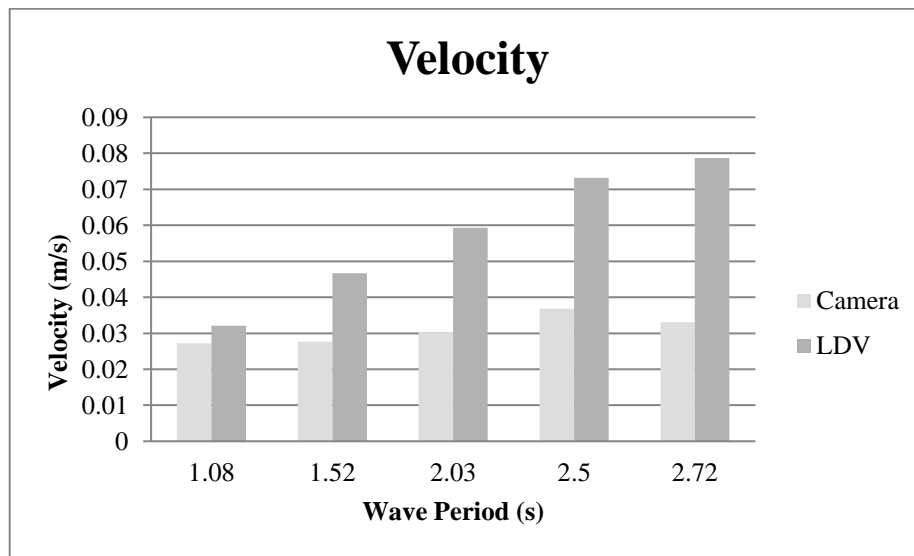
115 **Velocity**

116 The LDV records velocity, and the displacement data recorded by the camera

117 is used to derive its velocity. In figure 3, the RMS values of velocity for each

118 test are shown for both the motion camera and the LDV.

119



120

121 **Figure 3 RMS Velocity of Camera and LDV data**

122

123 Values recorded for the LDV are increasingly higher than those derived from  
 124 the camera for each successive test of increased wave period. The camera's  
 125 data here is inaccurate in that it doesn't increase proportionally with the  
 126 increase wave loading.

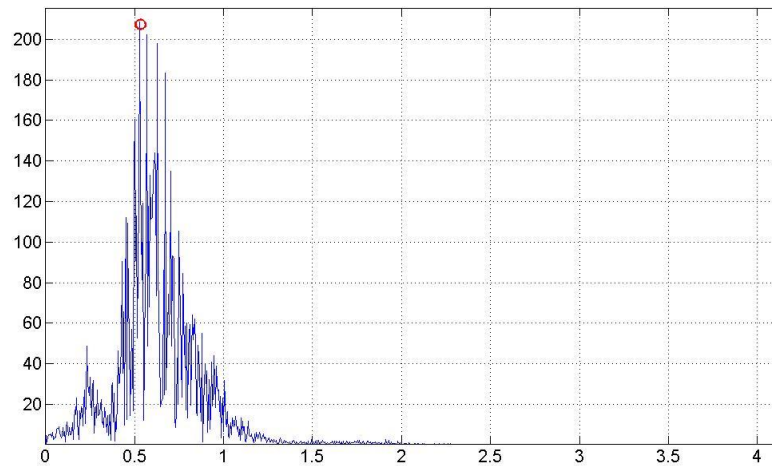
127

128 **Frequency**

129 The displacement time series for the LDV and the motion camera were  
 130 converted into the frequency domain with a Fourier Fast Transform (FFT).

131 The dominant input to the series, the waves acting are the dominant

132 frequency in this output, seen as the largest peaks (Figure 4).



133

134 **Figure 4 Fourier Fast Transform of Camera Displacement Time Series**

135

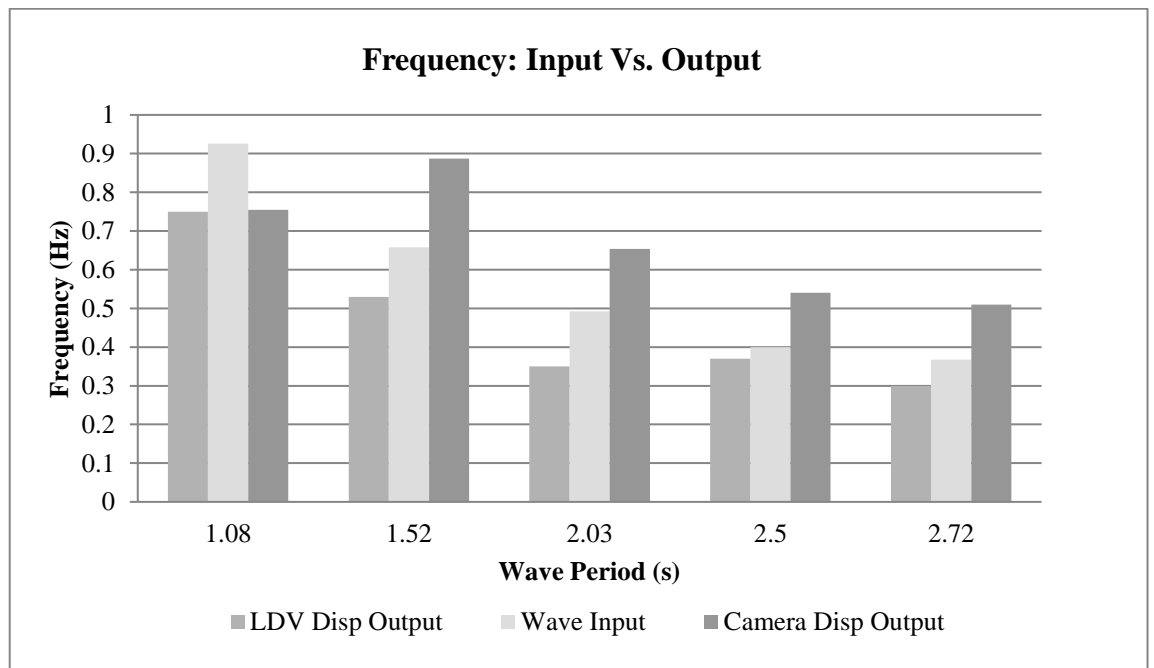
136 By comparing analysis outputs to known inputs for two different  
137 technologies, we can compare the retained accuracy of each. In Figure 4, the  
138 response of frequency of the output for the two different instrument is  
139 compared to the known frequency of the wave input to the system. The peak  
140 frequency of the velocity output of the LDV is, on average, 18.7% lower than  
141 the wave frequency of each particular test. Whereas the peak frequency of the  
142 camera's displacement is an average of 31.9% higher than the same inputs.

143

144

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146



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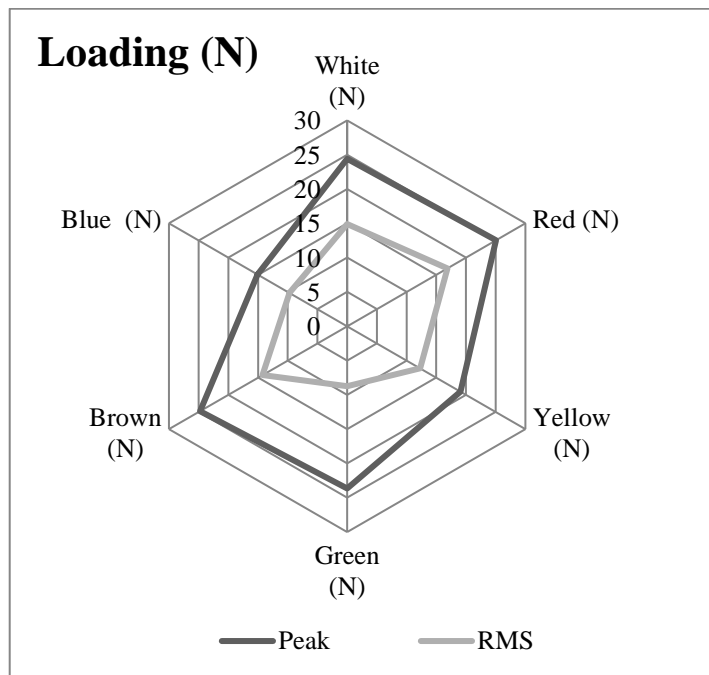
148 **Figure 5** Frequency comparison of input wave to frequency of LDV and camera  
 149 displacement outputs

150 The same comparison, but for the frequency of the LDV's velocity output  
 151 yielding a difference of only 7%, on average, from the wave input.

152 **Load Cells**

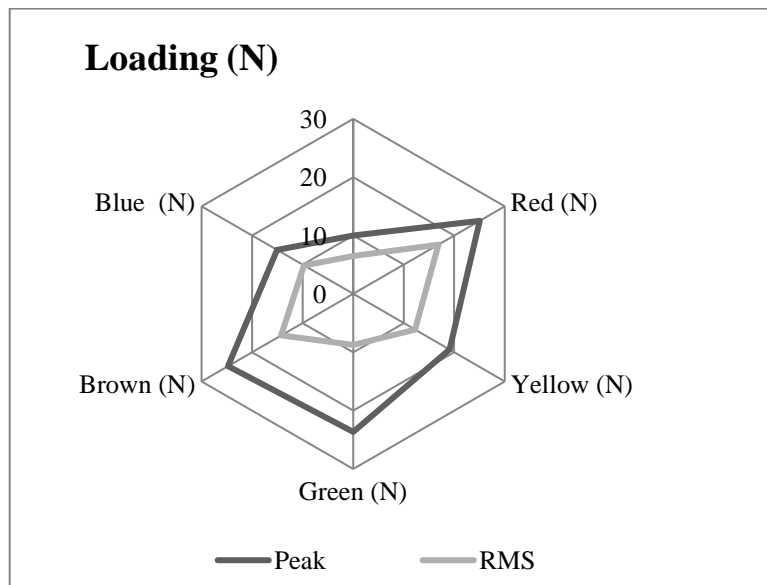
153 Load cells were placed at Bow Port, Bow Starboard, Mid Starboard, Stern  
 154 Starboard, Stern Port, Mid Port and were accordingly labelled White, Red,  
 155 Yellow, Green, Brown and Blue.

156 The average Peak and RMS load values for each load cell for 20 different  
 157 tests are represented in Figure 6. The highest loads are recorded in the  
 158 direction of the wave, at the bow and at the stern of the structure. Analysis of  
 159 the effect of removing different load cells to the overall data was carried out,  
 160 a sample of which is shown in Figure 7.



161

162 Figure 6



163

164 Figure 7

165 Data obtained from the white cell at Bow Port was removed, and the estimate  
166 shown for loading at this position shows a loss in accuracy of the loading on  
167 the structure.

#### 168 **4 Energy Aware Adaptive Sampling Algorithm for Energy** 169 **Harvesting WSNs**

170

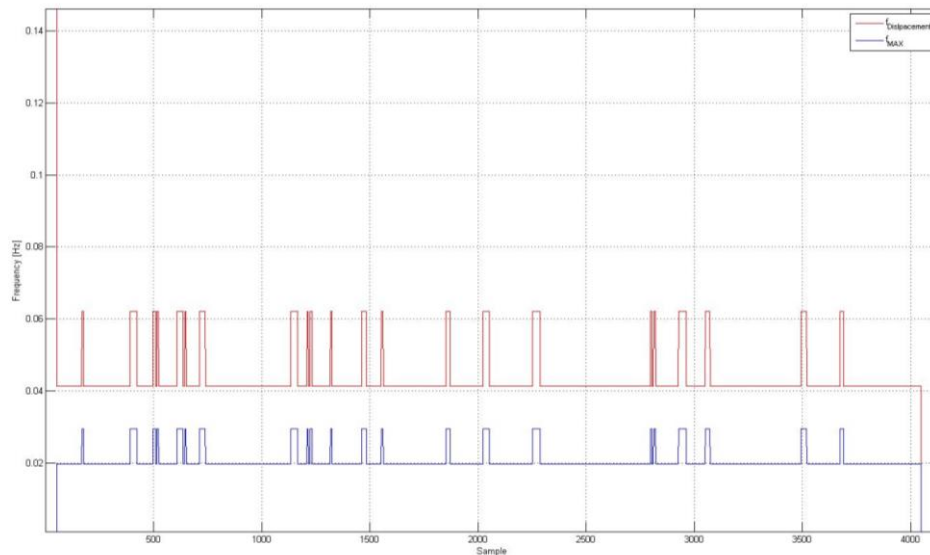
171 The development of WSNs technology is hindered by their limited energy  
172 supply. In the case of SHM applications, sensors are extremely expensive  
173 with respect to energy requirements. It is desirable to develop protocols that  
174 effectively manage the sensor power consumption while still meeting the  
175 requirements of the application. Adaptive sampling algorithms (ASA) are  
176 often used as a tool to minimize the communication between the sensor nodes  
177 within the network and at the same time to minimize the power consumed by  
178 the sensors by reducing the sampling rate according to the needs of the  
179 phenomenon observed.

180 An ASA presented in (Alippi et al., 2010) was implemented in Matlab and  
181 evaluated using data collected with sensor for **DISPLACEMENT** as recorded  
182 by the motion cameras.

183

184 The algorithm used evaluates the maximum frequency of the signal using  
185 FFT and then decides the sampling frequency by multiplying the maximum  
186 frequency with a constant which is  $\geq 2$  satisfying the Nyquist criterion. A

187 detailed description of the implemented algorithm with all relevant  
188 parameters explained can be found in (Alippi et al., 2010).



189

190 Figure 8 Matlab ASA Implementation of Camera Displacement Data

191 In figure 8, the sampling frequency according to the ASA and the maximum  
192 frequency of the signal are presented. The graph was generated by  
193 implementing ASA in Matlab with the following values for the relevant  
194 parameters:  $c = 2.1$ ,  $h = 5$ ,  $W = 50$ ,  $\delta = 0.1\%$ . Details for each of these  
195 parameters are explicitly given in (Alippi et al., 2010). The time between  
196 successive frames was 0.3125, thus the starting sampling frequency was  
197 32Hz. As shown in figure X, using the ASA reduces the number of acquired  
198 samples with respect to the traditional fixed sampling rate approach and  
199 hence saves energy.

200

201 **9 Discussions and Conclusions**

202 A comparison was made between high quality LDV data and lower quality  
203 motion camera data which recorded 3 different locations on the structure. It  
204 was initially thought that the multiple positions being tracked would increase  
205 accuracy, but due to physical characteristics of the mid mast location, the extra  
206 data was misleading of the overall structure and reduced overall accuracy of  
207 results. Fewer, better placed markers which took into account physical set up  
208 of model would have been more effective. However, for the load cells, a  
209 higher number of locations monitored leads to a better understanding of the  
210 structure under wave loading.

211 Section 4 deals with the optimisation the number of acquired samples to save  
212 energy. In applications where a battery powered system is used to interface a  
213 power hungry sensor, reducing the sampling rate when possible will extend  
214 the life of the battery while still maintaining the application data  
215 requirements. Dynamically changing the sampling frequency according to the  
216 needs of the phenomenon under observation can also improve the data  
217 quality. Using fixed sampling rate can cause undersampling of the signal,  
218 hence introducing error in the measurement and difficulties in reconstructing  
219 the signal and this method helps to avoid this.

220

221

222

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