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# Magnetic Ferrite / Carbonised Cotton Fibre Composites for Improving Electromagnetic Absorption Properties at Gigahertz Frequencies

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## ABSTRACT

Ferrite/carbon composited materials, especially the bio-derived composited materials possessing both environmental friendliness and outstanding microwave absorption performance, attract numerous attention for solving the “electromagnetic problem” in the Gigahertz frequency range. In this work, we demonstrate a bio-derived ferrite/carbon material by compositing functional carbonized cotton fibres (CCFs) and Fe<sub>3</sub>O<sub>4</sub> nanoparticles with optimized microwave-absorption properties. By adjusting the carbonization conditions systematically, the Fe<sub>3</sub>O<sub>4</sub> loading contents and the microwave absorption properties can be varied simultaneously – and, indeed, optimized and tuned. The CCFs-Fe<sub>3</sub>O<sub>4</sub> composites exhibited a minimum reflection-loss capacity  $RL(\text{dB})$  of -56.8 dB at 10.9 GHz with a thickness of 1.67 mm, and its effective absorption bandwidth ( $RL(\text{dB}) < -20$  dB) was found to broaden to 7.1 GHz. Electromagnetic characterizations, coupled with microstructure analyses, revealed that the enhancement in microwave absorption was triggered by the different microstructures of CCFs-Fe<sub>3</sub>O<sub>4</sub> composites - attributable to the different

carbonization processes. These different conditions result in different amounts of  $\text{Fe}_3\text{O}_4$  attachment sites and lead to the enhancement of dielectric polarisation at localized microstructures. The present work of bio-derived ferrite/carbon materials has important implications in understanding structure-performance relationships in dielectric-magnetic materials, and, meanwhile, could well be extended to a microwave-absorber design approach.

**KEYWORDS:** Electromagnetic absorption, bio-derived material, dielectric-magnetic composite, interfacial polarisation

## **Introduction**

In the past decade, electromagnetic problems - such as electromagnetic interference and pollution arising from applications in high-frequency technology - have become the main hazards to human health and aggravations to the quality of electronic communication<sup>1-5</sup>. In terms of electromagnetic-absorbing materials for attenuation of electromagnetic intensity as a means to tackle these problems, ferrites are most frequently used as owing to their cost effectiveness, excellent magnetic-loss properties, and good stability<sup>6</sup>. In this context, Yan *et al.*<sup>7-9</sup> have advanced the coordinated co-doping theory of multi-ions in ferrite, leading to the invention of power ferrites with the great scope and promise for the deployment of applications in the MHz-frequency band. Since then, various oxides have been investigated to further improve high-frequency performance<sup>10</sup>. It has been found that the single-phase structure, with refined single-domain grains, has been proven to serve as a prerequisite for high-frequency performance. Moreover, compositing ferrite with dielectric materials, such as ferrite/carbon,<sup>11, 12</sup> and ferrite/polymer<sup>13, 14</sup>, has shown excellent microwave-absorption performance in the Gigahertz frequency range. In such composite materials, microwave-absorption properties will be increased by integrating the dielectric loss (complex permittivity,  $\epsilon_r = \epsilon' - i\epsilon''$ ), magnetic loss (complex permeability,  $\mu_r = \mu' - i\mu''$ ), and impedance matching between

these<sup>15-17</sup>. In addition, the microwave-absorption properties of composite microwave-absorption materials, in particular the dielectric-loss capacity, could be further enhanced by substituting heteroatoms in the absorbents, to manipulate the electric-dipole polarisation behavior<sup>18-22</sup>. For example, Li *et al.*<sup>23</sup> reported that the microwave-absorption performance of Fe@C nanocapsules could be increased remarkably after substituted sulfur heteroatoms, ascribed to the formation of -C-S-C- and -C=S- heterostructures. Li *et al.*<sup>24</sup> synthesized the SiC doped Ni@C nanocapsules and found that the minimum reflection loss  $RL(\text{dB})$  could reach -49.99 dB at 5.12 GHz.

Although the microwave-absorption properties of such composited absorbents have been increased; however, the developments and applications are also hindered by several bottlenecks, such as high cost, complicated preparation approaches, and environment pollution<sup>25, 26</sup>. Thus, to overcome such blocks and increase microwave-absorption performance, carbonized bio-derived materials, such as cotton, wood, plant leaves, nutshell, and wheat straw, have been employed to act as dielectric-loss materials due to their low cost, favorable renewable-energy footprint, non-toxicity, lightweight nature, and environment-friendly performance<sup>27-30</sup>. Meanwhile, bio-derived materials also contain naturally multiple substituted elements, such as sulfur, nitrogen, phosphorus, and oxygen, which can serve to improve polarisation performance for multiple properties and result in the enhancement of dielectric-loss capacity. Hence, to leverage fully the advantages of bio-derived material and further modify their microwave-absorption properties, we demonstrate in the present work a bio-derived dielectric-magnetic material with compositing functional carbonized cotton fibres (CCFs) and  $\text{Fe}_3\text{O}_4$  nanoparticles. Notably, we find that microwave-absorption properties can be optimized and tuned by adjusting the carbonized conditions, attributed to the transformation of  $\text{Fe}_3\text{O}_4$ -loading contents and surface/interfacial microstructures of composite materials. In particular, for CCFs- $\text{Fe}_3\text{O}_4$  carbonized at 800 °C for 80 min, its minimum reflection loss capacity  $RL(\text{dB})$  reaches -56.8 dB at 10.9 GHz with a thickness of 1.67 mm,

and its effective absorption bandwidth ( $RL(\text{dB}) < -20 \text{ dB}$ ) is broadened to 7.1 GHz, exhibiting improved microwave-absorption properties.

## Results and discussion

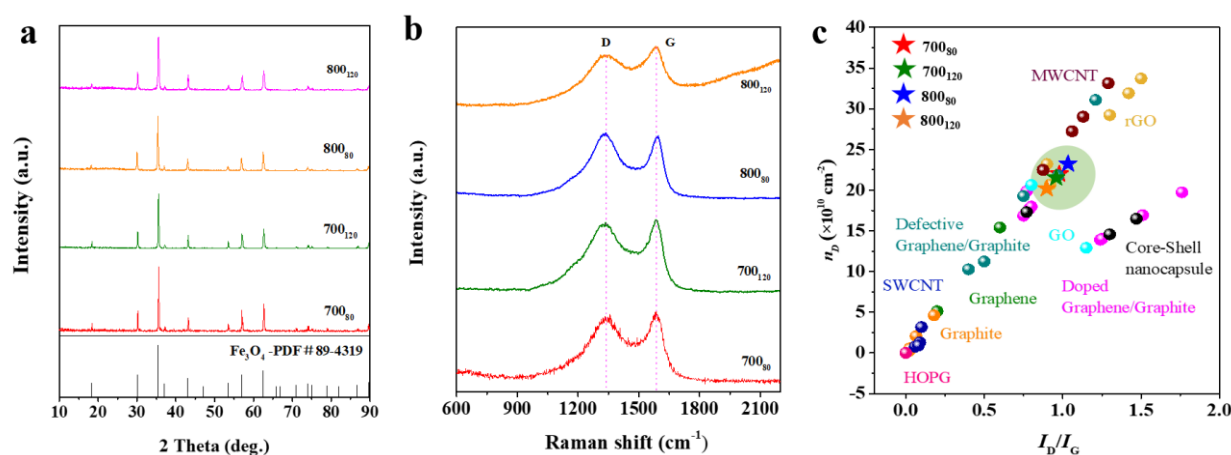
### *Microstructure characterisation*

Carbonized cotton fibres (CCFs) were treated at 700 °C and 800 °C for 80 min and 120 min, respectively, labeled as 700<sub>80</sub>, 700<sub>120</sub>, 800<sub>80</sub>, and 800<sub>120</sub>. The composite CCFs-Fe<sub>3</sub>O<sub>4</sub> were obtained by a hydrothermal method, which is outlined in some detail in the Experimental Section. **Fig. 1a** illustrates the X-ray diffraction patterns of different CCFs-Fe<sub>3</sub>O<sub>4</sub> samples, verifying that all of them are composed of the Fe<sub>3</sub>O<sub>4</sub> phase. Meanwhile, as the CCFs-Fe<sub>3</sub>O<sub>4</sub> is synthesised from a carbon-based skeleton, leading to a localized enlarged pattern exhibited in **Fig. S1**, which demonstrates the (006) peak of carbon fibres at ~26°. It can be discovered that different samples exhibit different intensity values, revealing that the degree of graphitisation and evolution of surface states have been changed after the carbonisation process. To further confirm the extent of graphitisation and intensity of defects, Raman spectra were employed as shown in **Fig. 1b** and **c**. For carbon-based materials, two peaks - the so-called D and G peaks - have always been observed. The D peak centered at ~1,350 cm<sup>-1</sup> was found to originate from the defective sp<sup>3</sup> bonds and the breathing mode of sp<sup>2</sup> bond in rings, whilst the G peak centered at ~1,580 cm<sup>-1</sup> originates from the sp<sup>2</sup> bonds<sup>31,32</sup>. Furthermore, the ratio between  $I_D$  and  $I_G$  is usually set as a function of defect intensity for carbon-based materials. Assisted by the  $I_D/I_G$  values, the concentration of defect sites ( $n_D$ ) was calculated by **Eq. (1)**<sup>33,34</sup>:

$$n_D(\text{cm}^{-2}) = \frac{(1.8 \pm 0.5) \times 10^{22}}{\lambda^4} \times \left(\frac{I_D}{I_G}\right) \quad (1)$$

in which  $\lambda$  (in nm) represents the wavelength of the Raman laser. For 700<sub>80</sub>, 700<sub>120</sub>, 800<sub>80</sub>, and 800<sub>120</sub> samples, the  $I_D/I_G$  and  $n_D$  values were found to be 0.98, 0.96, 1.03, 0.90 and  $2.20 \times 10^{11}$ ,  $2.15 \times 10^{11}$ ,  $2.32 \times 10^{11}$ ,  $2.02 \times 10^{11}$ , respectively. Under different carbonisation conditions, it could be realised that the defect intensity for different samples exhibits a slight difference. In particular, the CCFs-Fe<sub>3</sub>O<sub>4</sub> composites which are carbonised under 80 minutes exhibit higher

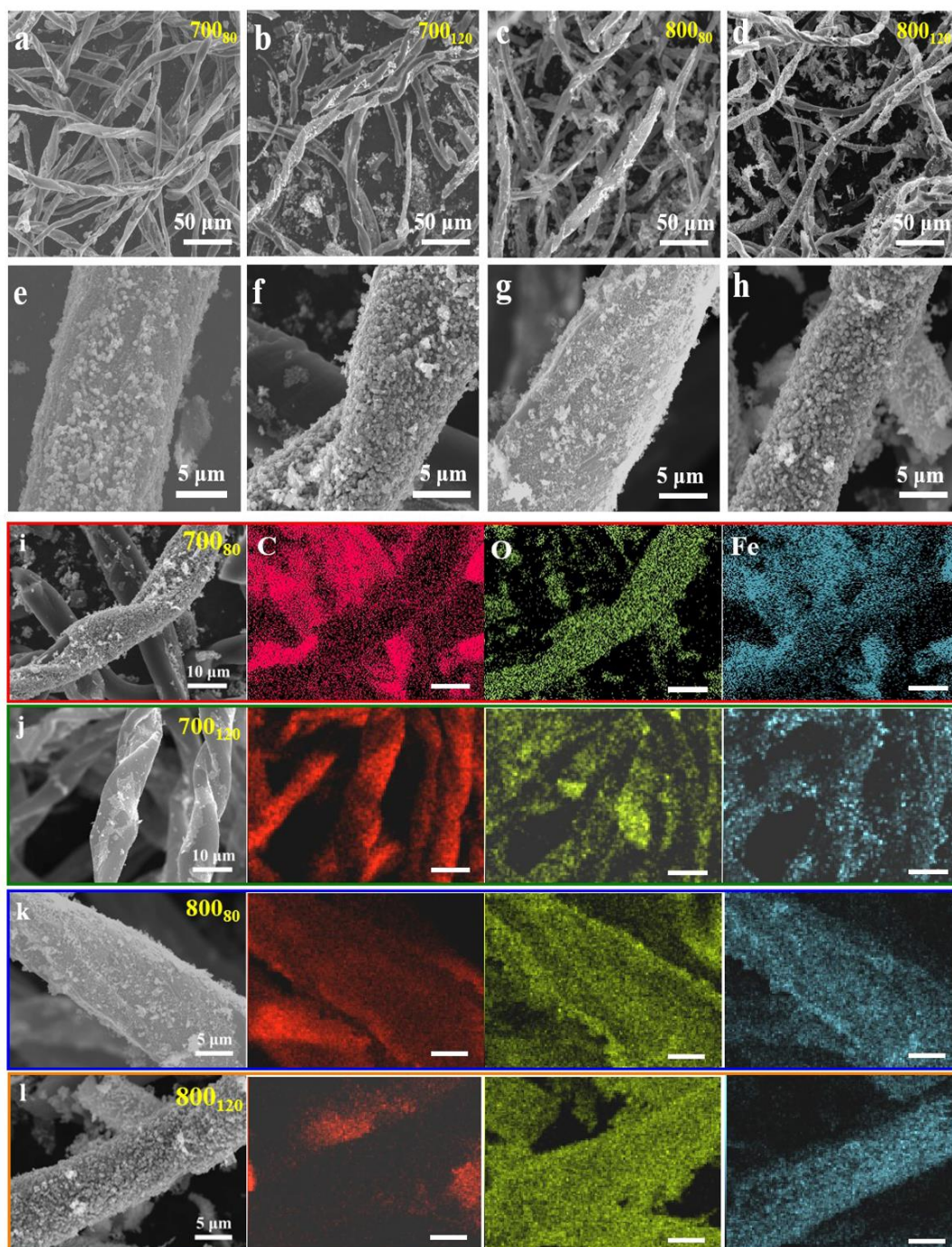
defect intensity than in 120 minutes. Such a different defect intensity could result from different carbonisation conditions, whilst the cotton fiber could convert more completely into carbon fibers when increasing the processing time, and thus increases the extent of graphitisation and decreasing defect intensity. Moreover, comparing with other carbon-based materials<sup>19, 21, 23, 35-43</sup>, it should be noted that the defect intensity of CCFs-Fe<sub>3</sub>O<sub>4</sub> composites are close to those of rGO, GO, and defective graphite/graphene materials - indicating a relatively high defect intensity in CCFs, triggered by heteroatom substitutions and vacancy defects.



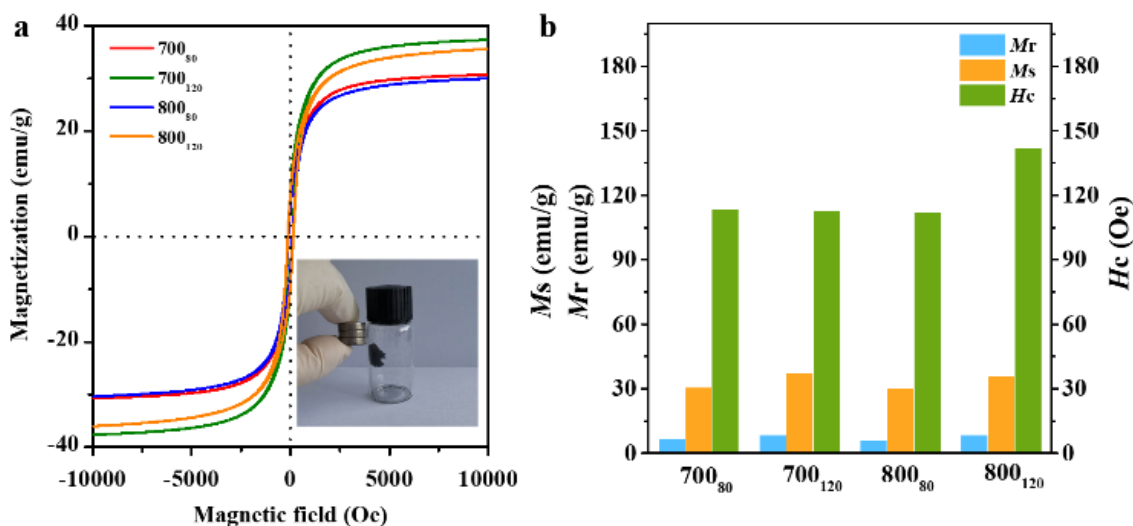
**Fig. 1** Characterisations of CCFs-Fe<sub>3</sub>O<sub>4</sub> composite. (a) XRD illustration, (b) Raman spectra, and (c)  $I_D/I_G$  values vs.  $n_D$  of different composites.

The microstructures were characterised initially using a scanning electron microscope (SEM), coupled with an energy-dispersive X-ray spectrum (EDX). SEM and high-resolution SEM images shown in **Fig. 2** confirm similar coating structures for four CCFs-Fe<sub>3</sub>O<sub>4</sub> composites. From the HR-SEM images in **Fig. 2e-h**, it has been proven clearly that the attachment quantity for Fe<sub>3</sub>O<sub>4</sub> nanoparticles exhibits a distinct difference. The CCFs samples which are carbonised for 80 minutes were found to exhibit relatively sparse nanoparticle-loading structures with numerous “banded” structures emerging at the surface. Furthermore, it can be noted that the cotton fibre has transformed into a twist shape with a diameter of ~8  $\mu\text{m}$

after a carbonised process. Such microstructural difference could be associated with the different extent of graphitisation of CCFs materials under different carbonised conditions, in which the  $\text{Fe}_3\text{O}_4$  binding sites on the CCFs surfaces have been modified and thus result in the changes of  $\text{Fe}_3\text{O}_4$  nanoparticle-loading contents. Meanwhile, the EDX-mapping images were employed to reveal the distributions of C (red), O (yellow), and Fe (cyan) in one individual fibre, as shown in **Fig. 2i-1**. It can be noted that the CCFs are coated by  $\text{Fe}_3\text{O}_4$  nanoparticles, in which the oxygen atoms not only exist in the  $\text{Fe}_3\text{O}_4$  nanoparticles but also substituted in the CCFs materials. Meanwhile, the magnetic properties would be changed with different  $\text{Fe}_3\text{O}_4$ -loading contents. As the VSM results show in **Fig. 3**, the magnetic property, especially the saturation magnetisation performance ( $M_s$ ), has been reduced under 80 minutes for the carbonisation process. Such behaviour owes to lower  $\text{Fe}_3\text{O}_4$ -loading contents, which have been revealed in SEM images.

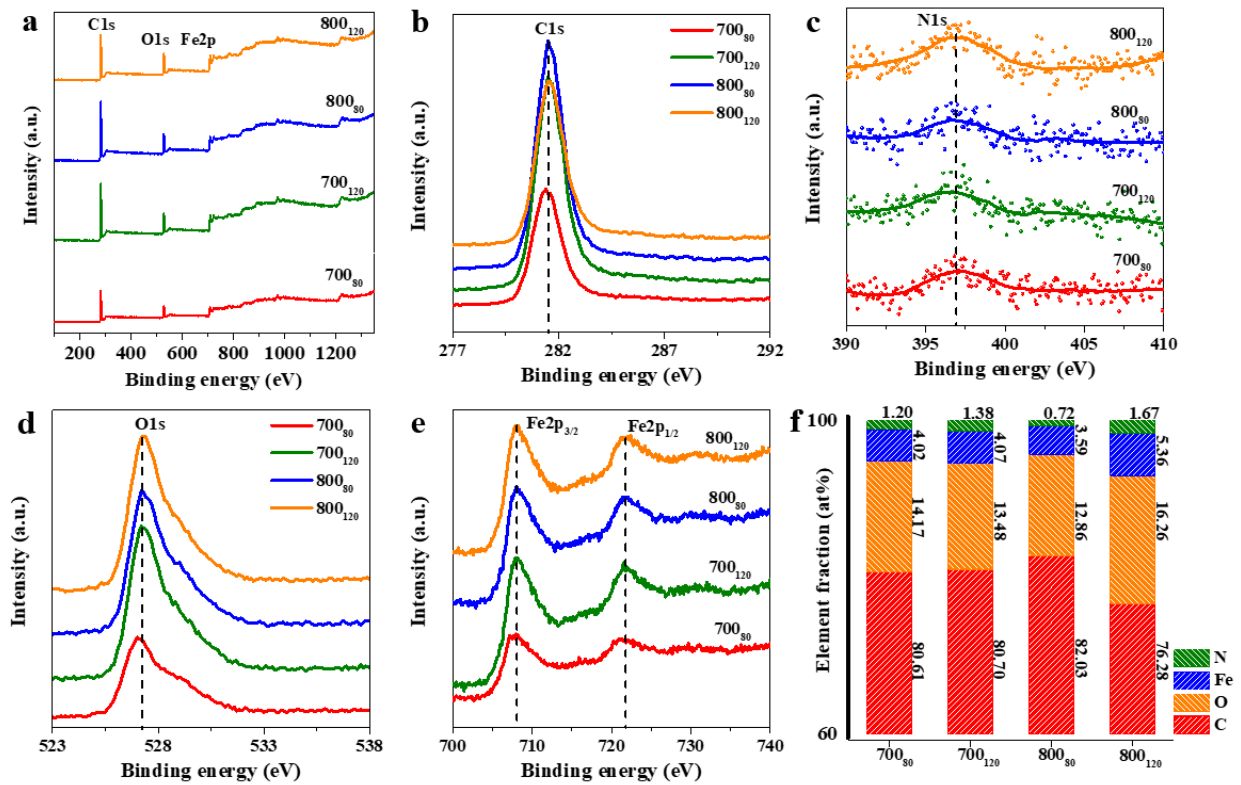


**Fig. 2** Microstructures of CCFs-Fe<sub>3</sub>O<sub>4</sub> composites. (a)-(d) SEM images of 700<sub>80</sub>, 700<sub>120</sub>, 800<sub>80</sub>, and 800<sub>120</sub> samples, (e)-(f) The corresponding high-resolution images, (i)-(l) The corresponding elemental C, O, and Fe mapping

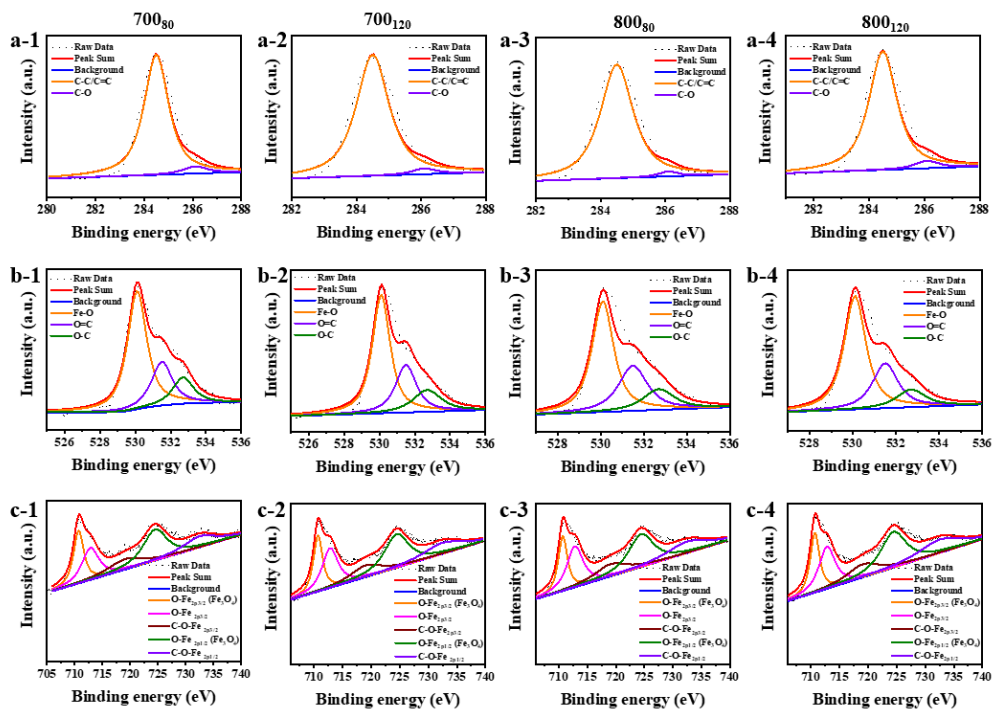


**Figure 3.** Magnetic properties of CCFs-Fe<sub>3</sub>O<sub>4</sub> composite. (a) Magnetic hysteresis loops, (b) Comparison of  $M_s$ ,  $M_r$ , and  $H_c$ .

The binding states and elemental distributions of different CCFs-Fe<sub>3</sub>O<sub>4</sub> composites are investigated by X-ray photoelectron spectroscopy (XPS) analyses, as shown in **Fig. 4** and **5**. Although the original cotton fibres could contain several different elements, in the present system it can be mainly detected as carbon, oxygen, nitrogen in CCFs and iron, oxygen in Fe<sub>3</sub>O<sub>4</sub> (**Fig. 4a** and **4c**). Based on XPS spectra, the binding states for C1s, O1s, and Fe2p have been investigated through software shown in **Fig. 5**. For O1s and Fe2p peaks, the spectra could be divided into Fe-O (O-Fe2p<sub>3/2</sub> and O-Fe2p<sub>1/2</sub>) for Fe<sub>3</sub>O<sub>4</sub> nanoparticles and O=C, O-C for CCFs skeletons. Moreover, the relatively elemental content for different composites has been summarised in **Fig. 4f**. It was found that the composite undergoing carbonisation for 80 minutes contained a lower oxygen content and higher carbon content, especially in the case of the 800 °C-carbonised composites, which could be attributed to the “banded” structures directly exposing inner CCFs skeleton in the XPS detection. Except for the carbon and oxygen contents, the substituted nitrogen elements exhibit slight changes for different samples, indicating little influence on microwave-absorption property.



**Fig. 4** XPS characterisations of CCFs-Fe<sub>3</sub>O<sub>4</sub> composite. (a) Survey spectra, (b) C1s spectra, (c) N1s spectra, (d) O1s spectra, (e) Fe2p spectra, and (f) The elemental content of different samples.



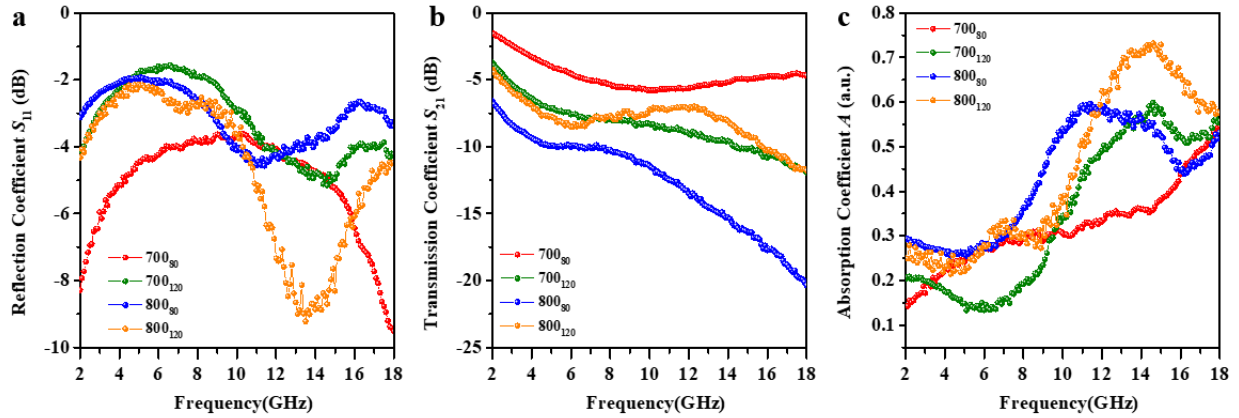
**Figure 5.** XPS characterisations of CCFs-Fe<sub>3</sub>O<sub>4</sub> composite with peak-fitting. (a) C1s spectra, (b) O1s spectra, (c) Fe2p spectra

### *Electromagnetic properties*

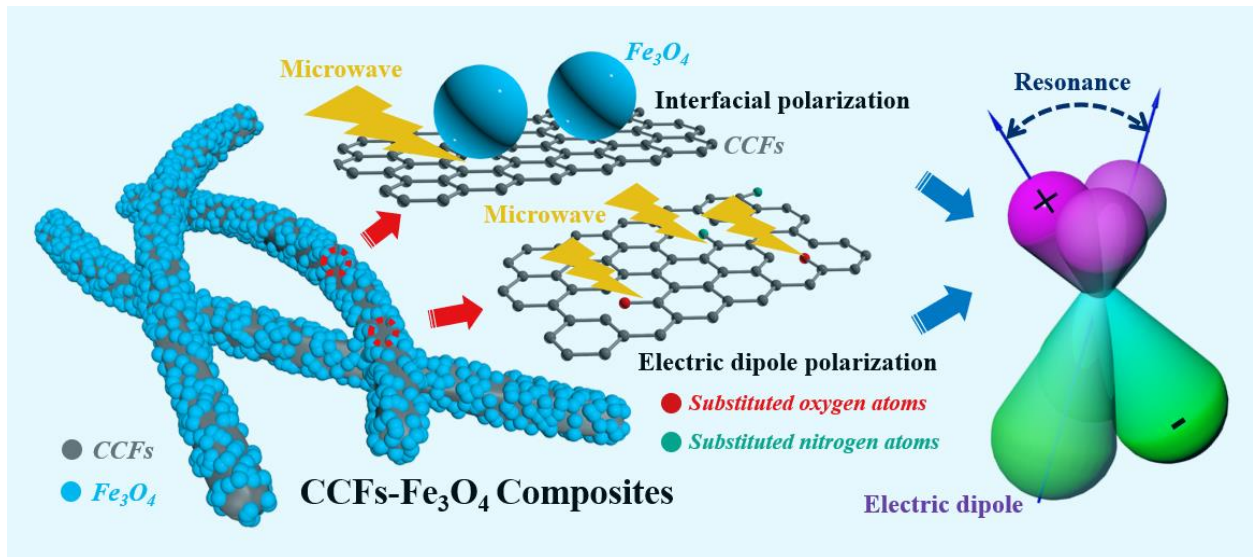
To investigate the microwave absorption properties of CCFs-Fe<sub>3</sub>O<sub>4</sub> composites, *S*-parameters ( $S_{11}$  and  $S_{21}$ ), which represent the reflection (*R*) and transmission (*T*) coefficients, have been evaluated by a vector network analyser (VNA) at 2-18 GHz. The absorption (*A*) coefficient which represents the absorption ability of different samples is calculated by **Eq. (2)** via *S*-parameters<sup>44,45</sup>.

$$A = 1 - |S_{11}|^2 - |S_{21}|^2 \quad (2)$$

As shown in **Fig. 6**, for *R* values, the 700<sub>120</sub>, 800<sub>80</sub>, 800<sub>120</sub>, the composites exhibit resonance peaks at 14.44, 11.08, and 13.56 GHz, respectively, in which the 800<sub>120</sub> composites provide the deepest resonance intensity amongst the four samples. For *T* values, the 800<sub>80</sub> composites were found to exhibit the lowest transmission performance amongst all four samples, and its coefficients exceed -20 dB above 16 GHz. For *A* values, it can be realised that the 800<sub>80</sub> composites exhibit a relatively high absorption performance before ~11 GHz, and the 800<sub>120</sub> composites display an optimised property at 11-18 GHz. This correlation phenomenon may be rationalised by the combination of reflection and transmission behavior, in which the 800<sub>80</sub> composites were found to exhibit the lowest  $S_{21}$  values, whilst the 800<sub>120</sub> composites present the deepest  $S_{11}$  resonance intensity, according to the calculated equation of the microwave-absorption coefficient.



**Fig. 6** Scattering parameters of CCFs-Fe<sub>3</sub>O<sub>4</sub> composite. (a) Reflection coefficient ( $S_{11}$ ), (b) Transmission coefficient ( $S_{21}$ ), (c) Absorption coefficient ( $A$ ).



**Fig. 7** Scheme of multi-polarisation behaviour, such as interfacial polarisation and electric-dipole polarisation of 800<sub>80</sub> composites.

To study in detail studied the electromagnetic-response performance for different samples, the relative complex permittivity ( $\epsilon'$ ,  $\epsilon''$ ) and permeability ( $\mu'$ ,  $\mu''$ ) were calculated form  $S$ -parameters by N1500A software (Keysight), as shown in **Fig. S2**. It is clear that 800<sub>80</sub> displays the largest  $\epsilon'$  and  $\epsilon''$  values amongst the four samples, in which the  $\epsilon'$  and  $\epsilon''$  correspond to the ability to store

energy and dielectric loss, respectively. The enhancement of dielectric-loss capacity could be associated with the surface microstructural difference caused by carbonisation, especially the non-dense Fe<sub>3</sub>O<sub>4</sub> coating structure (“banded” structure) which has been observed in HR-SEM image. Such a “banded” structure provides an inlet for microwave energy propagating in CCFs skeletons and further creates multi dielectric polarisation sites at the junction between CCFs skeleton and Fe<sub>3</sub>O<sub>4</sub> nanoparticle. Furthermore, the electric dipole would also be formed at natural heteroatom substituted sites such as oxygen and nitrogen elements. Under the external electromagnetic field, such dielectric polarisation behaviour serves to offset electromagnetic energy at a specific frequency, resulting in the enhancement of macroscopic dielectric-loss capacity. Consequently, in 800<sub>80</sub> composites, the electric dipole polarisation was found to be strengthened, owing to more microwave energy entering the interior of CCFs materials for dissipation through “banded” structures. This corresponding, specific loss behaviour is been illustrated in **Fig. 7**. In addition, to further understand the polarisation behaviour, the behaviour of Debye dipole polarisation - based on Cole-Cole “semicircle plots” - has been employed <sup>46</sup>:

$$\varepsilon_r = \varepsilon_\infty + \frac{\varepsilon_s - \varepsilon_\infty}{1 + j2\pi f\tau} = \varepsilon'(f) + i\varepsilon''(f) \quad (3)$$

$$\varepsilon'(f) = \varepsilon_\infty + \frac{\varepsilon_s - \varepsilon_\infty}{1 + (2\pi f)^2\tau^2} \quad (4)$$

$$\varepsilon''(f) = \frac{2\pi f\tau(\varepsilon_s - \varepsilon_\infty)}{1 + (2\pi f)^2\tau^2} \quad (5)$$

where  $\tau$  is the relaxation time,  $f$  is frequency,  $\varepsilon_s$  and  $\varepsilon_\infty$  stand for the stationary and optical dielectric constant, respectively. By integrating **Eq. (4)** and **(5)**, we obtain:

$$\varepsilon' = \frac{\varepsilon''}{2\pi f\tau} + \varepsilon_\infty \quad (6)$$

From **Eq. (6)**, it can be concluded that if dielectric loss is only influenced by electric-dipole polarisation, the plot of  $\varepsilon'$  verses  $(\varepsilon''/f)$  would be linear (**Fig. 8**). Each curve can be fitted by lines of different slopes - equal to the frequencies of Debye polarisations  $f_r$ . It can be noted that the polarisation behaviour for CCFs-Fe<sub>3</sub>O<sub>4</sub> composites could be divided into two parts: low-frequency polarisation (0.5-5 GHz) and high-frequency polarisation (5-40 GHz). Such polarisation phenomena can be rationalised as follow: (1) The  $\pi$  electrons in the material matrix lead to an asymmetric distribution of local electrons, thus forming an intrinsic dielectric polarisation at low frequencies<sup>47-49</sup>; (2) The natural N, P, S, O elements in CCFs, which are substituted originally in carbon fibres during carbonisation, result in a redistribution of charges to form electric dipoles<sup>23</sup>, and (3) Strong interface polarisation at the junction between Fe<sub>3</sub>O<sub>4</sub> and CCFs<sup>50</sup>, which occur at high frequencies. Moreover, for the magnetic loss capacity of different composites, the real and imaginary parts of the complex permeability depict a slight fluctuation. This implies that permeability depends mainly on Fe<sub>3</sub>O<sub>4</sub> nanoparticles, but contains a limit on loading content.

Based on this “transmit-line” theory, the reflection-loss capacity,  $RL(\text{dB})$ , versus frequency and thickness, can be expressed as **Eq. (7)**:<sup>51, 52</sup>

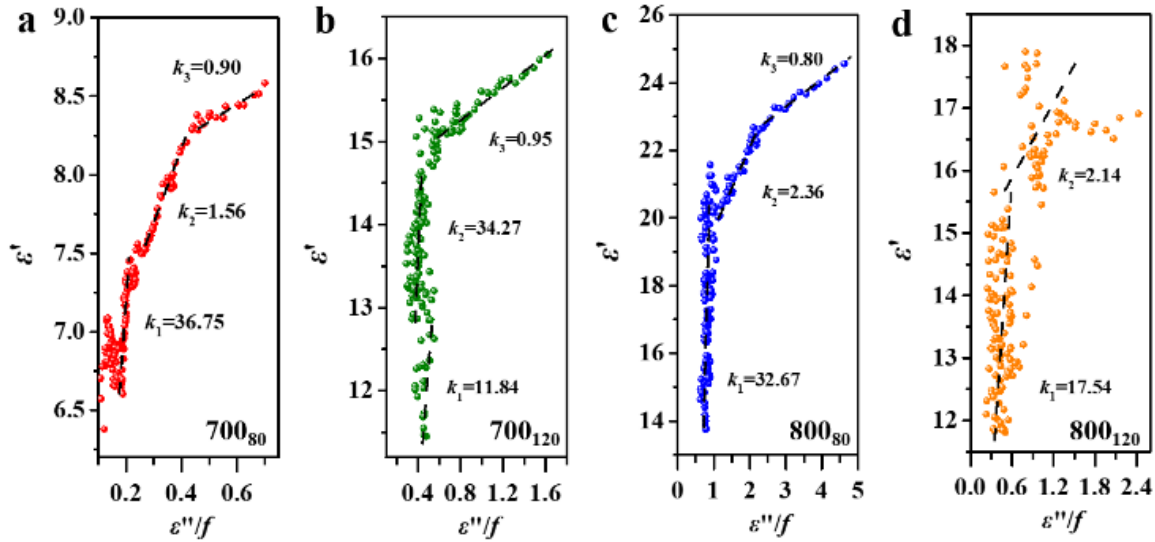
$$R(\text{dB}) = 20 \lg \left| \frac{Z_{in}-1}{Z_{in}+1} \right| \quad (7)$$

in which the normalised input impedance ( $Z_{in}$ ) of the absorber can be presented as **Eq. (8)**:<sup>52, 53</sup>

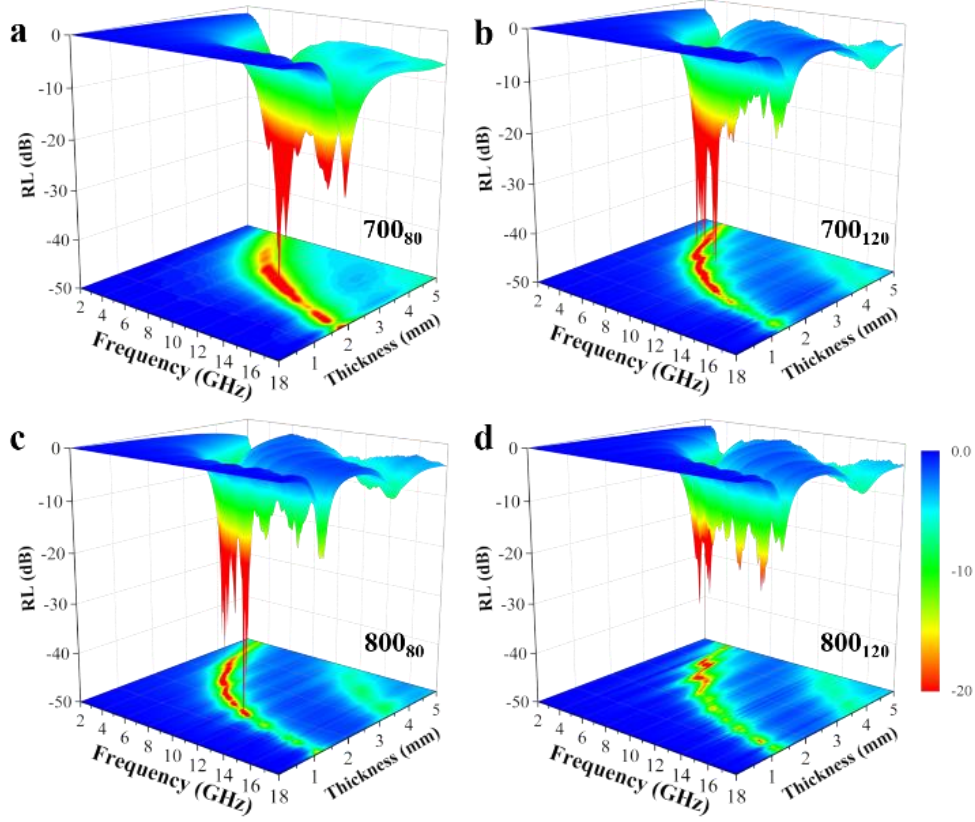
$$Z_{in} = \sqrt{\frac{\mu_r}{\varepsilon_r}} \tanh i \frac{2\pi f}{c} \sqrt{\mu_r \varepsilon_r} d \quad (8)$$

where  $c$  is the speed of light in free space,  $f$  is frequency, and  $d$  is the thickness of the absorber. When  $RL(\text{dB})$  is less than -20 dB, this indicates that more than 99% of electromagnetic energy has been dissipated. The corresponding frequency range for  $RL(\text{dB}) < -20$  dB can be regarded as

an effective absorption bandwidth. As **Fig. 9** shows, the effective absorption bandwidth for  $700_{80}$ ,  $700_{120}$ ,  $800_{80}$ , and  $800_{120}$  is 6.5 GHz, 6.6 GHz, 7.1 GHz, and 3.4 GHz, which centered at 8.5-13.6 GHz and 15.5-16.9 GHz, 5-11.6 GHz, 4.4-11.5 GHz, and 4.4-7.8 GHz, respectively. The minimised  $RL(\text{dB})$  values for four composites correspond to -61.05 dB, -47.72 dB, -56.81 dB, and -34.37 dB at 10.9 GHz, 6.7 GHz, 10.9 GHz, and 6.9 GHz, respectively. It is clear that the microwave absorption properties for  $800_{80}$  composites, especially the effective absorption bandwidth, have been enhanced by structural differences arising from the carbonisation process.



**Figure 8.** Cole-Cole plots of  $\epsilon'$  versus  $\epsilon''/f$  for CCFs- $\text{Fe}_3\text{O}_4$  composites.



**Fig. 9** 3D plots of microwave absorption ( $RL-f-d$ ) for CCFs- $Fe_3O_4$  composites. (a)  $700_{80}$  composites, (b)  $700_{120}$  composites, (c)  $800_{80}$  composites, (d)  $800_{120}$  composites.

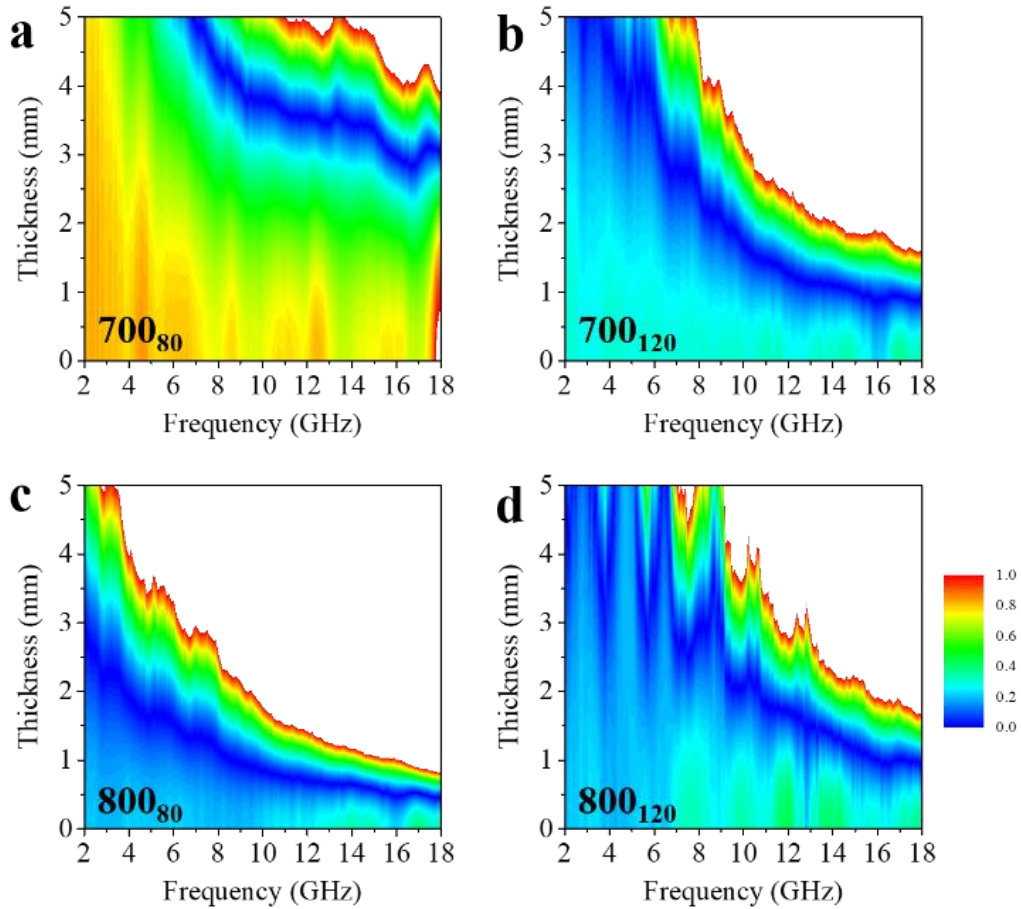
Moreover, the level of impedance matching,  $\Delta$ , has been determined by **Eq. (9)-(11)** and is exhibited in **Fig. 10**.<sup>54, 55</sup>

$$\Delta = |\sinh^2(kfd) - M| \quad (9)$$

$$k = \frac{4\pi}{c} \sqrt{\varepsilon' \mu'} \frac{\sin(\frac{\delta_E + \delta_M}{2})}{\sqrt{\cos(\delta_E) \cos(\delta_M)}} \quad (10)$$

$$M = \frac{4\varepsilon' \cos(\delta_E) \mu' \cos(\delta_M)}{(\mu' \cos(\delta_E) - \varepsilon' \cos(\delta_M))^2 (1 + \tan^2(\frac{\delta_M - \delta_E}{2}))} \quad (11)$$

where  $\delta_E$  and  $\delta_M$  represent the dielectric-loss angle and magnetic loss angle respectively. The matching degree  $\Delta < 0.4$  represents that the material contains good impedance matching. It is found that 800<sub>80</sub> composite contains a relatively small  $\Delta$  value in lower thickness among all 2-18 GHz than other composites, indicating a better impedance matching performance. It thus evidences that the microwave absorption property could be improved by the structural differences arising from carbonised conditions.



**Figure 10.** Impedance-matching degree  $\Delta$ : dependence on frequency for the CCFs-Fe<sub>3</sub>O<sub>4</sub> composites.

## Conclusion

In summary, we have prepared a bio-derived dielectric-magnetic material by compositing carbonised cotton fibres (CCFs) and Fe<sub>3</sub>O<sub>4</sub> nanoparticles, in which the CCFs have been carbonised at different temperatures and for different periods. Experimental results provide direct evidence for the microstructures and electromagnetic characterisations could be optimised and ‘tuned’ by adjusting carbonised conditions. Attributing to the “banded” structures, heteroatom substitutions, and Fe<sub>3</sub>O<sub>4</sub> coatings, the dielectric-loss capacity has been increased at 2-18 GHz, ascribed to the enhancement of dielectric polarisation at such localised microstructures. In particular, 800<sub>80</sub> composites exhibits the optimised *RL*(dB) of -56.8 dB at 10.9 GHz with a thickness of 1.67 mm, and its effective absorption bandwidth (*RL*(dB) <-20 dB) is broadened to 7.1 GHz. Considering the abundant natural resources, the present work not only proposes a new understanding of the structure-activity relationship but provides a new type of eco-friendly, high-performance microwave absorbers.

## **Experimental Methods**

*Preparation of carbon cotton fibres (CCFs)* The natural cotton was placed in a ceramic boat and then respectively heated to 700°C and 800°C in a quartz tube with a heating rate of 10 °C/min in Ar atmosphere. The annealed time was set at 80 min and 120 min, respectively. The obtained CCFs samples were labeled as 700<sub>80</sub>, 700<sub>120</sub>, 800<sub>80</sub>, and 800<sub>120</sub> in the following sections.

*Preparation of CCFs-Fe<sub>3</sub>O<sub>4</sub> composite* Fe<sub>3</sub>O<sub>4</sub> nanoparticles were prepared by a hydrothermal method<sup>56</sup>. Firstly, 4 mmol of FeSO<sub>4</sub>·7H<sub>2</sub>O was dissolved in 15 mL deionised water. After stirring (600 rpm) for 30 min, the solution was transferred into a Teflon-lined stainless-steel autoclave with a volume of 50 mL. Then, 4 mL of N<sub>2</sub>H<sub>4</sub>·H<sub>2</sub>O and 4 mL of NH<sub>3</sub>·H<sub>2</sub>O were added into the above solution. The solution pH value was adjusted to ~11. Then, the CCFs were added

into the mixed solution. After the reaction was carried out at 150 °C for 15 h in the oven, the system was naturally cooled to room temperature. The black precipitate was washed with deionised water and absolute ethanol several times. Finally, the prepared product was dried at 60 °C for 12 h.

*Microstructure characterisations* The crystal structure of the CCFs-Fe<sub>3</sub>O<sub>4</sub> was detected by X-ray diffraction (XRD) using CuK<sub>α</sub> radiation ( $\lambda=0.154$  nm). The morphology and elemental mapping were characterised by a scanning electron microscope (SEM) and energy-dispersive X-ray spectrum (EDS) (JEOL JSM-7001F field-emission scanning electron microscope). Raman spectra were recorded by a LabRAM HR Raman microscope with a laser wavelength of 532 nm. The surface element and chemical state were analysed by an X-ray photoelectron spectroscopy (XPS, Phoibos 100 spectrometer). The magnetic hysteresis loops were measured on a vibrating sample magnetometer (VSM, Lakeshore 7307) with a maximum magnetic field of 10 kOe at room temperature.

*Electromagnetic measurements* Electromagnetic parameters and scattering parameters (*S*-parameters) were measured by a vector network analyser (Keysight N5222A), which was calibrated by 2 port short-open-load-thru (SOLT) calibration standard (85054B) with a Type-N 50  $\Omega$  coaxial airline<sup>57</sup>. CCFs-Fe<sub>3</sub>O<sub>4</sub> composites were mixed uniformly with paraffin at a weight percentage of 30 wt.%, and then processed to a toroidal shape of 7.00 mm outer diameter and 3.04 mm inner diameter.

## AUTHOR INFORMATION

### **Author Contributions**

All authors have agreed to the manuscript.

## Notes

There are no conflicts of interest to declare.

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