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1 Sensor Measurement Strategies for Monitoring 2 Offshore Wind and Wave Energy Devices

3 Deirdre O'Donnell¹, Bruno Srbinovsky², Jimmy Murphy³ Emanuel Popovici²
4 and Vikram Pakrashi¹

5 **Abstract**

6 While the potential of offshore wind and wave energy devices is well
7 established in terms of environmental impact, operations and maintenance
8 issues are still not very well researched or understood. One of the important
9 aspects in this regard is the lack of access to these devices since they are
10 typically situated in high wind and wave conditions to generate more energy.
11 Consequently, deployment of sensors for such devices is an important issue
12 since they can measure the response of these devices in an as-deployed
13 condition and assessments or intervention decisions may be made based on
14 the fusion of data of such sensors and through the choice of intelligent
15 markers or modelling. While scaled model testing of devices in ocean basin
16 has gained popularity and wide acceptance over time, research in the
17 direction of developing guidelines for sensor measurement or placement
18 strategies are currently not in place. This paper addresses some specific
19 aspects of sensor choice, measurement and placement. In this regard, the
20 performances of the sensors are considered in terms of their receiver
21 operating characteristics (ROC) and uncertainties related to measurements are
22 addressed. The option of using multiple, cheaper sensors of seemingly
23 inferior performance as opposed to the deployment of a small number of

24 expensive and accurate sensors is also explored. Practical aspects of testing
25 are addressed in terms of exposure conditions and the performance of
26 different sensors. Tests have been carried out in an ocean wave basin and the
27 sensor placement for these tests has been used as a case study.

28 **1 Introduction**

29 Both offshore wind and wave energy technology has seen major advances in
30 recent years. Wave energy in particular is growing in popularity (Falcão
31 2010; Mccullen et al. 2002). Operations and maintenance (O&M) costs are a
32 highly relevant factor in the overall financial assessment of such projects, all
33 the more so in offshore projects due to lower availability of the device
34 (O'Connor et al. 2013). This has pushed the need for reliable structural
35 monitoring systems for accurate and reliable information about the health of
36 these energy conversion devices. With a move in recent times towards
37 offshore energy solutions, loss in ease of accessibility may lead to damage
38 going undetected, and the increased risk of catastrophic failure (Swartz et al.
39 2010).

40 There is clear financial benefit to optimizing time between inspections and
41 scheduled maintenance work, which affects the uptime of systems while also
42 coming with their own costs- an unscheduled maintenance event is five times
43 more costly than one that is scheduled (Adams et al. 2011). However, high
44 costs related to some sensing systems outweigh the benefits to O&M cost
45 savings so the value of expensive sensing systems must be evaluated.

46 There are many forms of sensing systems, based on various technologies.
47 Accelerometers have been successfully applied to identifying and locating the
48 presence of structural damage in offshore structures (Mangal 2001), as well
49 as motion cameras and load cells (V.JAKSIC; ref; ref) and Fiber Bragg

50 Grating (FBG) to measure strain. Cameras can even be employed in
51 underwater situations to detect damage (O'Byrne et al. 2014) where marine
52 growth exasperates fatigue damage. However, little is known of the relative
53 merits of these technologies.

54 Wireless sensor networks (WSN) are a promising technology which have in
55 recent years gained much attention from academia and industry alike. The
56 application of WSN technology to structural health monitoring (SHM) has
57 the potential to provide a substantial and quantifiable improvement to
58 existing monitoring solutions for civil infrastructure (Boyle et al. 2011)
59 .While wired SHM systems would require more maintenance and more
60 frequent site visits as wires can be damaged over time, wireless SHM systems
61 offer flexibility, even on difficult to access structures, and significantly
62 reduced costs of installation and maintenance.

63 However, some of the existing wireless systems for SHM still have high
64 power consumption. The high power consumption and the limited power
65 budget make these systems unsuitable for long-term installation on a structure
66 and requires frequent site visits for system maintenance.

67 WSN nodes are battery powered and because of their limited energy source
68 they are not suitable for long-term structural health monitoring applications.

69 With the focus on enhancing the life time of a wireless sensor node, a popular
70 is by complementing an energy harvesting technique with an efficient energy
71 management algorithm (Sharma et al. 2010). This approach has the potential

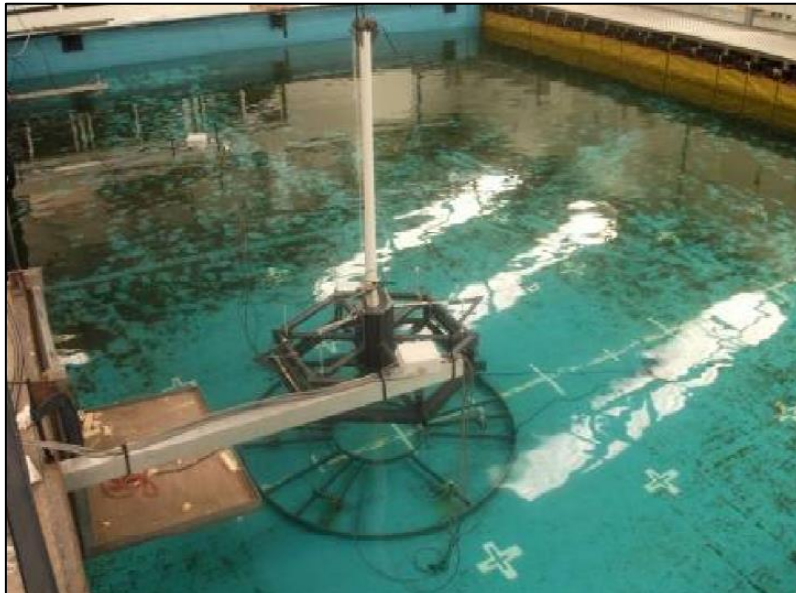
72 to achieve self-sustainability of the node with harvesting energy from the
73 environment and effectively managing the node activity (i.e. the sampling
74 rate of the sensors) according to the energy levels and the dynamics of the
75 phenomenon observed (Srbinovski et al. 2015unpublished)

76

77 **2 Experimental Model**

78 **2.1 Model**

79 A scaled Tension Leg Platform (TLP), a truss like structure with a hexagonal
80 base, was tested in this study. This device consists of a gravity base
81 connected by six mooring tethers to the Buoyancy Ring and the Upper
82 Structure and the Tower and Nacelle, all as shown in fig 1.



83

84

Figure 1 TLP Model

85

2.2 Instrumentation and Testing

86 The model was instrumented with 6 Tedeo-Huntleigh stainless steel single
87 ended bending beam load cells which were attached to the six mooring line
88 cables and bolted to the gravity base. These measured the cable tension in
89 Newtons (N). The instantaneous positions of 3 reflective markers, which
90 were attached to the six corners of the hexagonal base, were monitored by 4
91 Qualisys 3-Series Oqus Marker Tracking Cameras with a sampling frequency
92 of 32Hz. A Laser Doppler Vibrometer (LDV) was also employed during
93 testing to record the velocity of the TLP. This high resolution technology
94 samples at a rate of 480 Hz. Displacements and velocities were recorded in the
95 wave direction, as this was considered the most critical plane.

96 The model was tested at the Hydraulics and Maritime Research Centre
97 (HMRC), University College Cork (UCC), Ireland in its Ocean Wave Basin.
98 A variety of periods and wave amplitudes were used and the Bret Schneider
99 wave spectrum was chosen, to best represent a true sea state.

100

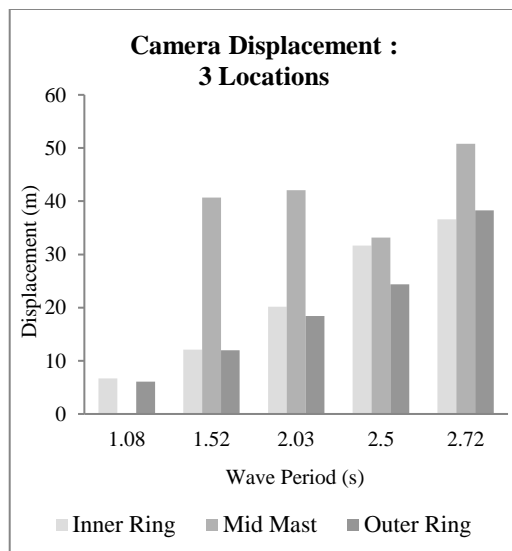
101 **3 Results**

102 **Displacement**

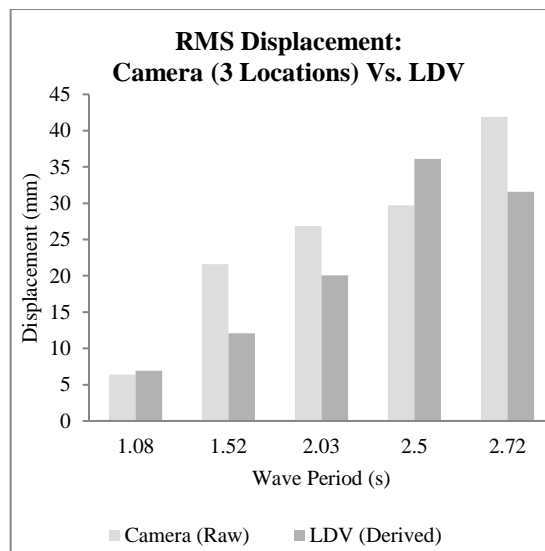
103 The camera recorded the position of the TLP at 3 different locations; the
104 Inner Ring, the Outer Ring and the Middle Mast. The velocity of the structure
105 as recorded by the LDV was used to find displacement values.

106 Figure 2(a) shows the displacements recorded by the camera at the 3 tracked
107 positions. Due to the far larger amplitude of displacement at the mid mast
108 position, due to the flexible nature of the mast and its sensitivity, these
109 readings were omitted from the average value shown in figure 2 (c), as they
110 were viewed to be skewing the data (see figure 2 (b)).

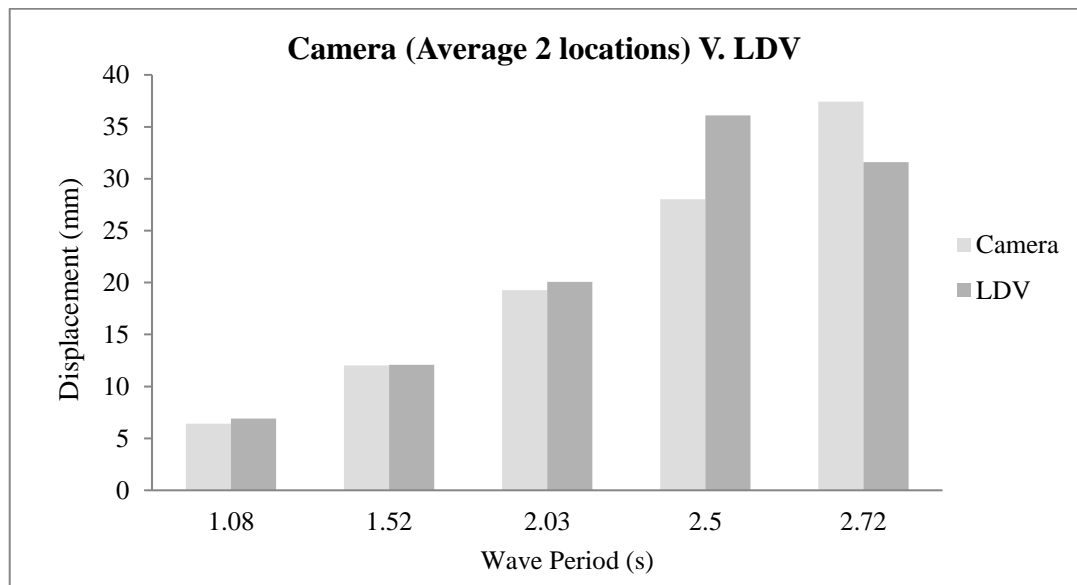
111



2(a)



2(b)



2(c)

112 **Figure 2 Displacement**

113

114

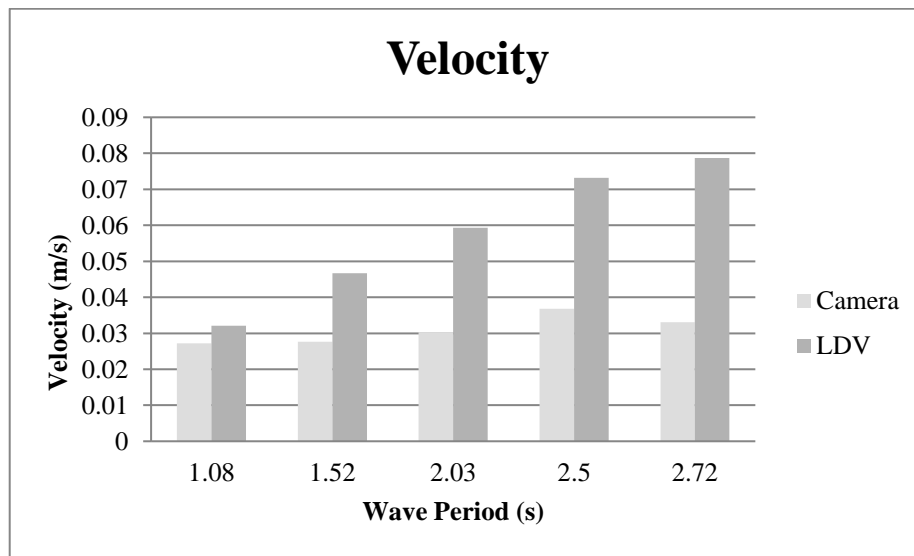
115 **Velocity**

116 The LDV records velocity, and the displacement data recorded by the camera

117 is used to derive its velocity. In figure 3, the RMS values of velocity for each

118 test are shown for both the motion camera and the LDV.

119



120

121 **Figure 3 RMS Velocity of Camera and LDV data**

122

123 Values recorded for the LDV are increasingly higher than those derived from
 124 the camera for each successive test of increased wave period. The camera's
 125 data here is inaccurate in that it doesn't increase proportionally with the
 126 increase wave loading.

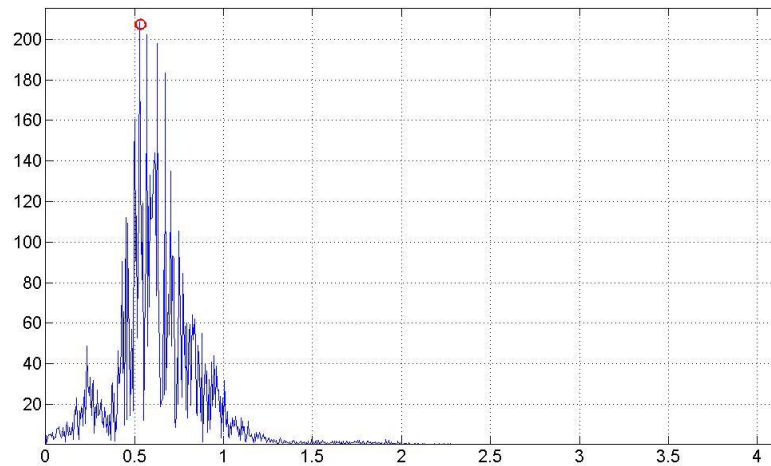
127

128 **Frequency**

129 The displacement time series for the LDV and the motion camera were
 130 converted into the frequency domain with a Fourier Fast Transform (FFT).

131 The dominant input to the series, the waves acting are the dominant

132 frequency in this output, seen as the largest peaks (Figure 4).



133

134 **Figure 4 Fourier Fast Transform of Camera Displacement Time Series**

135

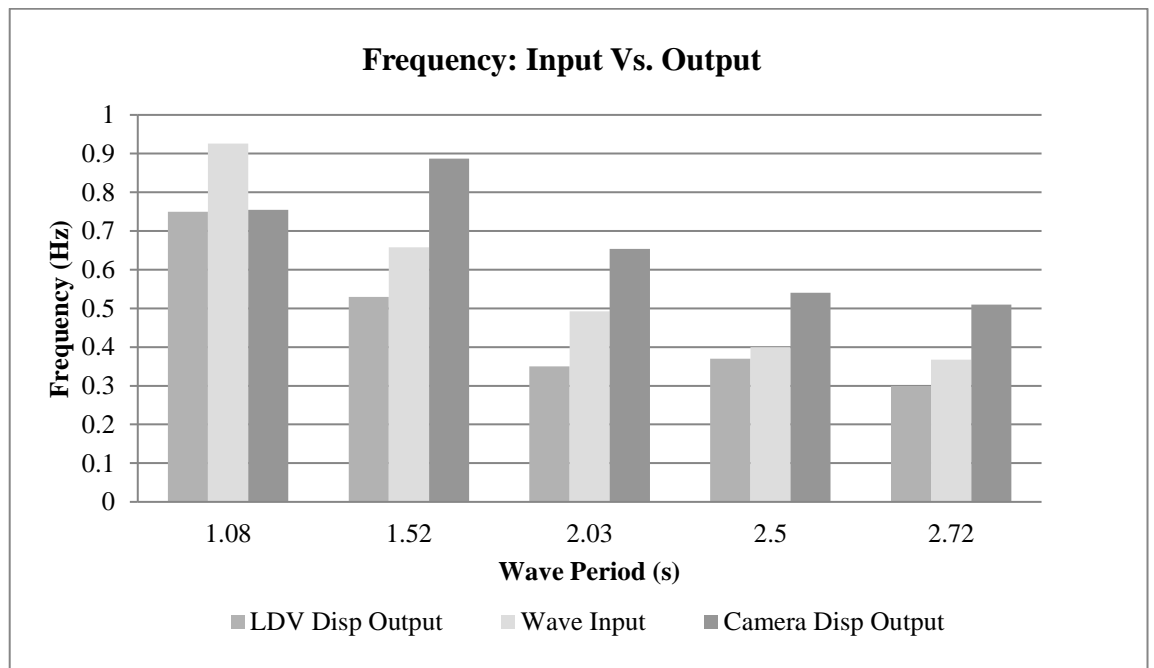
136 By comparing analysis outputs to known inputs for two different
137 technologies, we can compare the retained accuracy of each. In Figure 4, the
138 response of frequency of the output for the two different instrument is
139 compared to the known frequency of the wave input to the system. The peak
140 frequency of the velocity output of the LDV is, on average, 18.7% lower than
141 the wave frequency of each particular test. Whereas the peak frequency of the
142 camera's displacement is an average of 31.9% higher than the same inputs.

143

144

145

146



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148

149

Figure 5 Frequency comparison of input wave to frequency of LDV and camera displacement outputs

150

The same comparison, but for the frequency of the LDV's velocity output

151

yielding a difference of only 7%, on average, from the wave input.

152

Load Cells

153

Load cells were placed at Bow Port, Bow Starboard, Mid Starboard, Stern

154

Starboard, Stern Port, Mid Port and were accordingly labelled White, Red,

155

Yellow, Green, Brown and Blue.

156

The average Peak and RMS load values for each load cell for 20 different

157

tests are represented in Figure 6. The highest loads are recorded in the

158

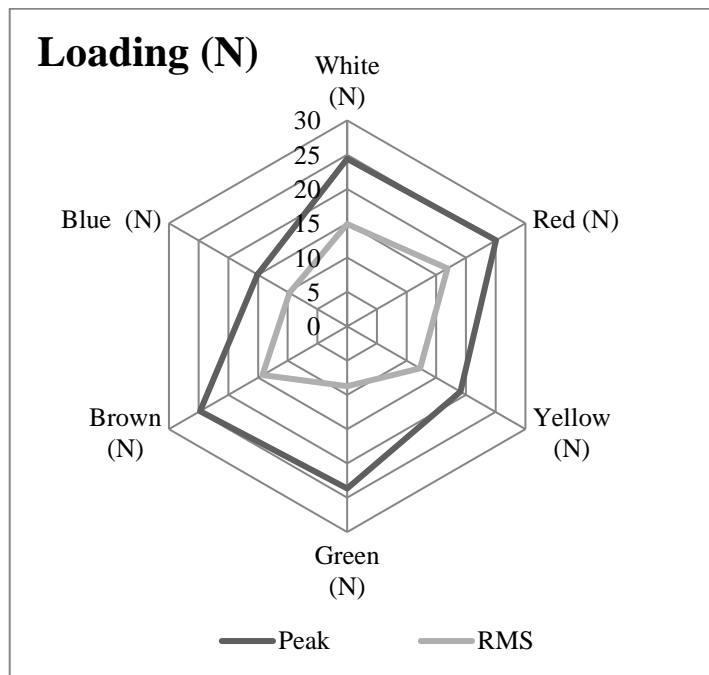
direction of the wave, at the bow and at the stern of the structure. Analysis of

159

the effect of removing different load cells to the overall data was carried out,

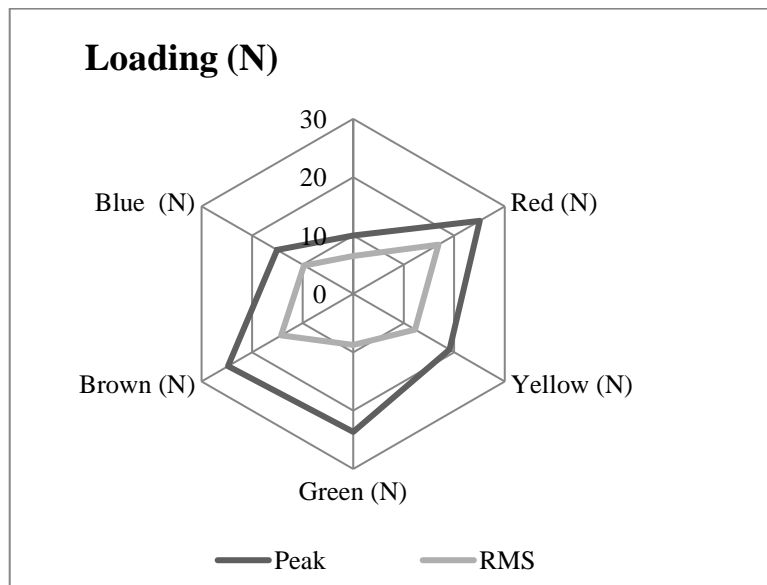
160

a sample of which is shown in Figure 7.



161

162 Figure 6



163

164 Figure 7

165 Data obtained from the white cell at Bow Port was removed, and the estimate
166 shown for loading at this position shows a loss in accuracy of the loading on
167 the structure.

168 **4 Energy Aware Adaptive Sampling Algorithm for Energy** 169 **Harvesting WSNs**

170

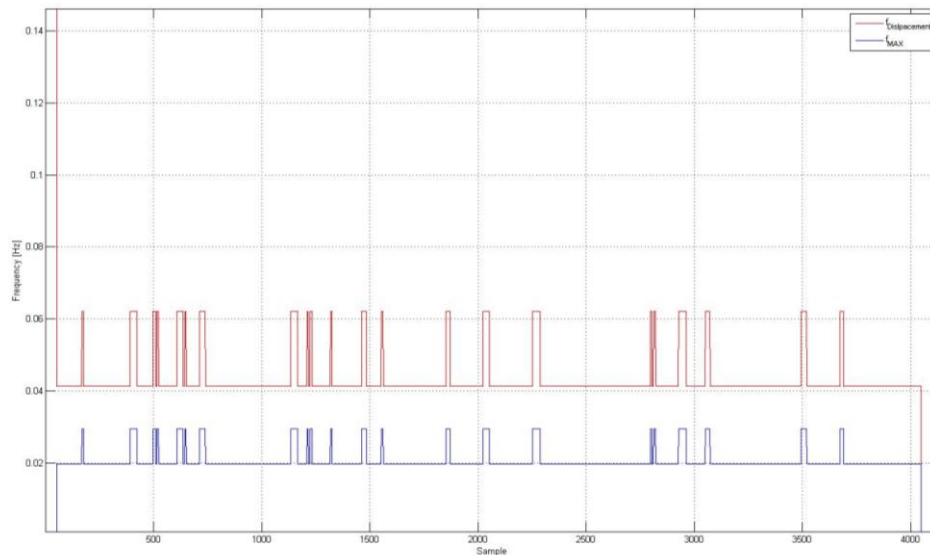
171 The development of WSNs technology is hindered by their limited energy
172 supply. In the case of SHM applications, sensors are extremely expensive
173 with respect to energy requirements. It is desirable to develop protocols that
174 effectively manage the sensor power consumption while still meeting the
175 requirements of the application. Adaptive sampling algorithms (ASA) are
176 often used as a tool to minimize the communication between the sensor nodes
177 within the network and at the same time to minimize the power consumed by
178 the sensors by reducing the sampling rate according to the needs of the
179 phenomenon observed.

180 An ASA presented in (Alippi et al., 2010) was implemented in Matlab and
181 evaluated using data collected with sensor for **DISPLACEMENT** as recorded
182 by the motion cameras.

183

184 The algorithm used evaluates the maximum frequency of the signal using
185 FFT and then decides the sampling frequency by multiplying the maximum
186 frequency with a constant which is ≥ 2 satisfying the Nyquist criterion. A

187 detailed description of the implemented algorithm with all relevant
188 parameters explained can be found in (Alippi et al., 2010).



189

190 Figure 8 Matlab ASA Implementation of Camera Displacement Data

191 In figure 8, the sampling frequency according to the ASA and the maximum
192 frequency of the signal are presented. The graph was generated by
193 implementing ASA in Matlab with the following values for the relevant
194 parameters: $c = 2.1$, $h = 5$, $W = 50$, $\delta = 0.1\%$. Details for each of these
195 parameters are explicitly given in (Alippi et al., 2010). The time between
196 successive frames was 0.3125, thus the starting sampling frequency was
197 **32Hz**. As shown in figure X, using the ASA reduces the number of acquired
198 samples with respect to the traditional fixed sampling rate approach and
199 hence saves energy.

200

201 **9 Discussions and Conclusions**

202 A comparison was made between high quality LDV data and lower quality
203 motion camera data which recorded 3 different locations on the structure. It
204 was initially thought that the multiple positions being tracked would increase
205 accuracy, but due to physical characteristics of the mid mast location, the extra
206 data was misleading of the overall structure and reduced overall accuracy of
207 results. Fewer, better placed markers which took into account physical set up
208 of model would have been more effective. However, for the load cells, a
209 higher number of locations monitored leads to a better understanding of the
210 structure under wave loading.

211 Section 4 deals with the optimisation the number of acquired samples to save
212 energy. In applications where a battery powered system is used to interface a
213 power hungry sensor, reducing the sampling rate when possible will extend
214 the life of the battery while still maintaining the application data
215 requirements. Dynamically changing the sampling frequency according to the
216 needs of the phenomenon under observation can also improve the data
217 quality. Using fixed sampling rate can cause undersampling of the signal,
218 hence introducing error in the measurement and difficulties in reconstructing
219 the signal and this method helps to avoid this.

220

221

222

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