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Wind Power Scenario Tree Tool: Development and Methodology

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Abstract—Driven by a trend towards renewable forms of generation, in particular wind, the nature of power system operation is changing. With respect to wind power, the uncertainty of the wind becomes an issue which must be considered. Through the use of wind forecasting, this uncertainty may be managed. The error inherent in forecasting will impact system reliability and cost as will inaccuracies in assumptions about the forecast error. This paper presents the methodology adopted for use in a Scenario Tree Tool constructed to allow for closer examination of the effect of forecast error assumptions and properties in unit commitment scheduling models.

Index Terms—Wind power generation, Forecast error, Stochastic Unit Commitment

I. INTRODUCTION

THE nature of power system operation is changing worldwide. Plans are in place to increase the proportion of demand met through wind power throughout the European Continent [1], Ireland [2], Great Britain [3] and the United States [4]. In Europe, for example, this change is driven by EU policy which aims to reduce CO₂ emissions and dependency on imported fuel. Primarily this policy encourages the growth of renewable generation including wind power [5]. It is expected that this increase in renewable generation will displace conventional generation - causing a decrease in system operation costs as less conventional fuel is consumed in meeting system demand.

However, displacing conventional generation with non-synchronous renewable generation is creating new system operation challenges. Wind is by its nature variable. It is of limited predictability and control of the resource is limited to curtailment. As wind cannot be forecast with perfect accuracy, additional reserve must be carried and conventional units must be operated in a more flexible, adaptable manner - leading to reduced efficiency through partial loading and an increase in the number of start-ups required for conventional power plants

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Fig. 1. Illustration of rolling planning Scenario Trees

[6]. While the effects of this uncertainty can be disregarded for low wind penetrations, with high wind penetrations the uncertainty associated with wind forecasting error will impact upon the reliability, efficiency and economic performance of unit commitment [7].

While stochastic treatments of wind uncertainty have previously been investigated, the contribution to solution quality of specific statistical properties of forecast error have not been considered. These properties are available from analysis of the error between historical forecasts and realised data. In ideal circumstances, a system operator will have the necessary information prioritised in the form best suited for decision making. In practice, and in many prior studies quantification of forecast error has often been limited to simple statistical properties such as variance and mean error and an assumed Gaussian distribution [9].

The WILMAR project developed a stochastic unit commitment scheduling model to analyse the integration of wind power in a large liberalised electricity system [8]. The WILMAR scheduling model uses a rolling sequence of scenario tree forecasts to model the impact of error information (see Fig.1) This model has previously been used to study

the benefits of stochastic treatment of wind uncertainty over deterministic treatments as well as the impact of accounting for more of the wind uncertainty by increasing the frequency of rolling planning [7].

This paper presents the methodology adopted for use in a Scenario Tree Tool (STT) constructed to allow for closer examination of the effect of forecast error assumptions and properties when combined with a suitable unit commitment model such as WILMAR. Due to the requirement for direct control of the statistical properties in several areas of interest, ARMA series/scenario reduction methodologies were not considered suitable for this tool. A new STT was designed using a methodology based upon a moment matching technique where each time period, within a tree, has a defined variance, skewness and kurtosis. These statistics together with the autocorrelations of the scenario determine the values of the scenarios at that time period. While alternative heuristic methodologies have been proposed for deriving a scenario tree that matches specific moments [10], the methodology used in this tool is based upon a nonlinear optimisation moment matching method [11], [12].

Section II describes the methodologies related to the STT. It Details the program structure and methodologies (moment matching and scenario grouping) used to generate wind and load scenarios within the current STT as well as the method used to account for diurnal/seasonal variations. In addition to describing the new methodology, it also briefly describes the preceding scenario reduction/ARMA series method which was used by older versions of the STT.

Section III covers the methodologies used for calculating the replacement reserve, the amount of reserve required to be available after a short delay, from these trees as well as detailing, for completeness, the assumptions about spinning reserve, the amount of reserve required to be available from online generators at a given time, and the semi markov chain methodology used to simulate forced outages as required by the replacement reserve methodology.

Section IV displays example graphical outputs from the preceding sections.

A conclusion is presented in Section V.

II. DEVELOPMENT AND METHODOLOGY OF THE SCENARIO TREE TOOL

In power plant scheduling, decisions must be made on both information known with certainty and uncertain information which must be forecasted. In stochastic unit commitments, wind forecasts, demand forecasts and their forecast error can be accounted for by representative branching trees consisting of probability weighed scenarios for available wind generation (Fig. 1). The number of scenarios has been restricted to minimise dimensionality in the unit commitment solution, while retaining accuracy in the specified statistical information. For computational reasons, the first stage of these trees is assumed to be known with perfect certainty.

Each scenario in the tree consists of an assigned probability and two time series values - one for load and one for wind.

Fig. 2. Structure of the Scenario Tree Tool.

Each of these time series can be represented as a forecast time series, common to all scenarios within the tree, and an error time series which, together with the error time series of the other scenarios, represents the error distribution of the forecast.

In the All Island Grid Study (AIGS), these scenario trees were generated by an STT using a methodology based upon scenario reduction of ARMA series [14]. In brief, Scenario Reduction aims to take an initially large number of scenarios and then remove scenarios until only the desired number remain while maintaining as close a representation of the original distribution as possible according to the methodology given here in brief:

- 1) Generate 1000 36 period Wind Speed scenarios using Arma (1,1) Series of equal probability.
- 2) Calculate the Kantorovich distance between each pair of scenarios.
- 3) Merge the probability of the scenarios with the lowest Kantorovich distance and delete the scenario of smaller probability.
- 4) Repeat steps 2 and 3 until the desired number of scenarios is achieved.
- 5) To create the branching scenario tree, this process is repeated omitting the hours in the third stage to reduce the scenarios further.
- 6) These remaining scenarios are added to the wind speed forecast and converted to wind power scenarios using the aggregated wind power curve.

Due to the requirement for direct control of the statistical properties in several areas of interest, ARMA series/scenario reduction methodologies were not considered suitable for

this tool. A new STT was designed using a methodology based upon a moment matching technique where each time period, within a tree, has a defined variance, skewness and kurtosis. These statistics together with the autocorrelations of the scenario determine the values of the scenarios at that time period. While alternative heuristic methodologies have been proposed for deriving a scenario tree that matches specific moments [10], the methodology used in this tool is based upon a nonlinear optimisation moment matching method [11], [12].

The overall structure of the Scenario Tree Tool (STT) can be seen in Fig.2 where W is wind scenarios, L is load scenarios and P is the probability of each scenario. Each functional box represents a separate module or submodule in the STT which will be covered in the subsequent sections. Entries on the same level represent parallel operations which can be run simultaneously. The steps in brief follow and can be seen graphically in Fig.3:

- 1) Set initial parameters and begin from the final stage of the tree
- 2) Generate the scenarios for the current stage of the tree using moment matching. (II.A)
- 3) Calculate the degree of similarity between each subset (size determined by the ratio of branching) in terms of Kantorovich distance and autocorrelations. (II.B)
- 4) Generate an optimal branching structure between the current stage and its predecessor using the subsets which minimise the disparity between merging scenario branches.
- 5) Repeat the preceding steps for the earlier stages using the branching structure and scenario values as further inputs into the objective function (1).

A. Moment Matching

For each stage in the tree, a nonlinear optimization was used to produce a matrix of scenarios consisting of wind, demand and probability values matching the specified statistics as closely as possible. In addition, stages which have already been determined are used to provide additional autocorrelation information for subsequent stages.

In each stage, the optimisation acts to minimize the following objective function (1) while meeting the constraints (4, 5, 6) given the stages and branch connections that have already been defined:

$$\sum_{n=1}^S W_n (f_n(x_t, P_t) - S_n)^2 \quad (1)$$

S is the set of statistical properties under consideration. W_n is the optimisation weight assigned to the statistical property. S_n are the components of the set S (mean, variance, kurtosis, skewness, first four autocorrelations). $x_{t,j}$ is the set of values for scenario j during the given time step t . P_t are the probabilities assigned to the scenarios in time step t .

The individual components ($f_n(x)$) of the objective function (1) are calculated using the following formulas for the moment

Fig. 3. Structure of the Scenario generation

(2) and autocorrelation (3):

$$M_l = \sum_{j=1}^s P_j (x_{j,t} - \mu_t)^l \quad (2)$$

$$AC_{\tau,j} = \sum_{j=1}^{N-\tau} \frac{(Y_i - \mu_j)(Y_{i+\tau} - \mu_j)}{\sum_{j=1}^N (Y_i - \mu_j)^2} \quad (3)$$

M_l is the l th Moment at time t . $AC_{\tau,j}$ is the autocorrelation at timelag τ for scenario j . μ_t is the mean of the scenario set at time t . μ_k is the mean of the scenario k and τ the time lag of the autocorrelation. k is the index of a given scenario. jk are the indices of the scenarios which branch from scenario k .

In order to ensure probability remains consistent across scenarios and time periods, the constraints upon the objective function are as follows:

$$\sum P_{jk,t} = P_{k,t-1} \quad (4)$$

$$\sum P_t = 1 \quad (5)$$

$$P_{jk,t} > 0 \quad (6)$$

B. Scenario Grouping

The scenario stages produced by moment matching are divided into groupings according to the branching of the scenario tree and the similarity of their autocorrelations. This is done to ensure that when joined to the relevant scenario in the preceding stage the autocorrelation of each branch of the tree is consistent across the stage boundaries. This prevents the creation of suboptimal scenario branching as a result of

joining two disparate scenarios. Scenario ordering is determined by finding the ordering which minimises the difference in autocorrelation and the Euclidean distance between the short term (stage II) values of each scenario .

$$D(j1, j2) = \sum_{t=1}^T \frac{(x_{j1,t} - x_{l,t})^2}{(x_{j2,t})^2} + \sum_{z=1}^{\tau} \frac{(AC_{\tau,j1} - AC_{\tau,j2})^2}{(AC_{\tau,j1})^2} \quad (7)$$

These groupings and scenarios are then used in the optimisation of any subsequent moment matching steps to provide consistent autocorrelations for each scenario throughout the tree stages.

C. Diurnal and Seasonal variation

Wind and load forecasts exhibit different behaviour at different times of the year and day. In order to account for seasonal and diurnal variation, the error trees can be altered before being added to the individual forecasts by the addition of a mean error adjustment time series, $\mu(j)$ to each scenario and the use of a scaling constant ϵ .

The values of $\mu(j)$ and ϵ are chosen through fitting the general forecast error to the forecast error of each seasonal period and time period within the day. This is achieved by subdividing the known forecast information by seasonal period, calculating the same metrics as the main data and deriving the necessary adjustments from the proportional difference in standard deviation and mean between the general case and the specific case. This process is repeated for the starting hour of the forecast to derive the adjustment for time of day.

III. REPLACEMENT RESERVE AND FORCED OUTAGES

A. Replacement Reserve

Replacement reserve is estimated for each individual scenario branch of wind and demand within the tree and is calculated using a similar methodology to that presented in the AIGS [14]. However, the AIGS used methods assuming prior scenario reduction, which calculate reserve from the 90th percentile of the unreduced set of scenarios used to generate the scenario tree. This method can therefore not be used with the new STT as the new methodology uses moment matching and does not generate the large initial number of scenarios required by the AIGS methodology. Instead, the reserve is calculated from the 90th percentile of a distribution based upon the variation of wind and demand error represented by those scenarios (8) according to the following method:

The n scenario combinations are mapped onto the wind scenario s from which they came and the reserve is taken to be the 90th percentile of the difference between the reference power balance $P_{Ref}(9)$ and the forecasted power balance, P , for the scenario combinations n at each wind scenario s (10):

$$\Delta P(t_0, f, s) = P_{Ref}(t) - P(t_0, f, s) \quad (8)$$

Fig. 4. Algorithm for forced outage calculation

The power balance P_{Ref} at time t is calculated for the realised values of wind W_R , load L_R and available conventional capacity C :

$$P_{Ref}(t) = \sum_{g \in G} C(g) + W_R(t) - L_R(t) \quad (9)$$

The power balance P of each combination of wind and load scenarios n is calculated for the scenario Wind W_E and Load L_E as well as the forced outages. and time t is calculated for the realised values of wind W_R , load and available conventional capacity C :

$$P(r, t_0, f, n) = \sum_{g \in G} C(g) Y(g, t) + W_E(t_0, f, n) - L_E(t_0, f, n) \quad (10)$$

Fig. 5. Example autocorrelated scenario, thin line, imposed onto scenario tree points. Deterministic forecast is shown by the thick line, realised value is shown by the thick dashed line.

Fig. 6. Scenario tree with inverted skewness. Note the tree is skewed to the opposite side of the deterministic forecast.

In addition to this, required spinning reserve is estimated from the largest infeed to the system and forecasted wind using the methodology presented in the AIGS [9].

B. Forced Outages

While no new changes have been made to this methodology, it is included here for completeness as it is necessary for the reserve calculations as well as being a required input for the unit commitments it is currently in use with. Within the model, distinction is drawn between two types of outage (forced outages and scheduled outages). As scheduled outages are defined by the user and by the test system, the STT simulates forced outages from the information provided about the test system including the information provided on scheduled outages.

The time series of forced outages for each conventional unit are simulated using semi-markov chains [13], where the failure and repair rates are expressed by the mean time to failure and the mean time to repair. The methodology used in the STT is derived from that presented in the All Island Grid Study (AIGS) [14] and is detailed in brief below.

$$P_{Available} = \frac{MTTF}{MTTR + MTTF} \quad (11)$$

$P_{Available}$ is the probability that a plant will be available derived from the Mean Time to Failure ($MTTF$) and Mean

Fig. 7. Example un-autocorrelated scenario, thin line, imposed onto scenario tree points. Deterministic forecast is shown by the thick line, realised value is shown by the thick dashed line.

Fig. 8. Scenario tree with increased kurtosis. Note the increase in points clustered at the mean and at the extremes

time to Repair ($MTTR$) for each plant.

$$P_{Unavailable} = \frac{MTTR}{MTTR + MTTF} = FOR \quad (12)$$

$P_{Unavailable}$ is the probability that a plant will be unavailable and is equivalent to the Forced Outage Rate (FOR).

$$FOR = \frac{t_{fo}}{t} \quad (13)$$

t_{fo} is the total number of hours the plant is unavailable and t is the total time period.

Fig. 4 shows the structure of the forced outages algorithm. The initial state of the unit is determined by drawing a random number from a uniform distribution and comparing it to the Full outage percentage (FOP) calculated according to equation 14.

$$FOP = \frac{FOR}{MTTR} \quad (14)$$

The result of this determines whether or not the model will draw a time to repair (TTR) or a time to failure (TTF) from the Weibull distribution.

$$f(t, \mu, k) = \frac{k}{\mu} \left(\frac{t}{\mu}\right)^{k-1} \cdot e^{-\left(\frac{t}{\mu}\right)^k} \quad (15)$$

Where the shape factor $k = 1$ is used for the TTF (as time to failure is captured by an exponential distribution), $k = 5$ is used for the TTR (time to failure represented by a bell shaped

Fig. 9. Scenario tree with decreased kurtosis. Note the reduction in clustering and the more even spread of points

distribution) and μ is calculated from $MTTF$ and $MTTR$ respectively.

IV. RESULTS

This section presents example scenario tree outputs from the STT to demonstrate the impact of altering statistics.

Fig. 5 gives an example of the points contained in a statistically accurate scenario tree overlayed upon the realised and forecasted values (thick dashed line and line respectively). In addition, a single scenario is shown (thin line with squared points) to demonstrate the impact of including autocorrelation in the optimisation.

Fig. 7 presents a tree constructed from identical information without autocorrelation considered. Due to this, the included scenario in this version contains considerably more sharp changes than the reality entails. As a result, despite the statistics of each individual time period being correct, the grouped scenarios do not present useful information.

Fig. 6 presents the same tree with inverted skewness. While it is similar in shape to Fig. 5, its shape appears transposed around the forecast as its skewness is of the opposite sign. The scenario tree constructed in this fashion assumes the opposite trend in terms of overestimating or underestimating the forecast.

Fig. 8 demonstrates the effect of reducing kurtosis - a tree which is clustered closer to the forecast with an increased number of extreme values.

In contrast Fig. 9 demonstrates the effect of reducing kurtosis - a tree which is comparatively evenly spread throughout the distribution.

V. CONCLUSION

This paper presented the methodology of the Scenario Tree Tool based upon moment matching. Example output demonstrating some of the converted to a graphical format were also included. This tool is under development to examine the impact of wind forecast error statistics upon unit commitment for high wind penetration test systems.

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