Developing a method for soft gamma-ray Laue lens assembly and calibration

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Abstract

Laue lenses constitute a promising option for concentrating soft gamma rays with a large collection area and reasonable focal lengths. In astronomy they could lead to increased telescope sensitivity by one to two orders of magnitude, in particular for faint nuclear gamma-ray lines, but also for continua like hard X-ray tails from a variety of compact objects. Other fields like Homeland security and nuclear medicine share the same need for more sensitive gamma-ray detection systems and could find applications for gammaray focusing optics. There are two primary challenges for developing Laue lenses: the search for high-reflectivity and reproducible crystals, and the development of a method to accurately orient and fix the thousands of crystals constituting a lens. In this paper we focus on the second topic. We used our dedicated X-ray beamline and Laue lens assembly station to build a breadboard lens made of 15 crystals. This allowed us to test our tools and methods, as well as our simulation code and calibration procedure. Although some critical points were identified, the results are very encouraging, with a crystal orientation distribution lower than 10'', as required to build a Laue lens telescope dedicated to the study of Type Ia supernovae (30-m focal

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length). This breadboard lens represents an important step towards raising the technology readiness level of Laue lenses.

Keywords: Telescope, Soft gamma rays, Laue lens, Focusing optics, Crystals, Technological development

1 1. Introduction

Observations of the sub-MeV gamma-ray sky enable direct glimpses of 2 fundamental physics processes involving conditions that are not reproducible 3 in the laboratory, such as extreme magnetic fields up to 10^{15} G near magne-4 tized neutron stars or extreme gravitational fields near black holes. However, 5 observations are hampered by the limited sensitivity of current telescopes. 6 High instrumental background in detectors is the main problem, and building bigger detectors is not a viable solution as the sensitivity only (roughly) 8 scales with the square root of the detector surface area. A Laue lens telescope q (LLT) allows the decoupling of the collecting area from the detector area, dra-10 matically increasing the signal-to-noise ratio and hence the sensitivity. The 11 benefits of focusing high-energy radiation was recently demonstrated once 12 again with NASA's observatory NuSTAR extending the focused bandpass to 13 80 keV [1] (the maximum was previously ~ 12 keV). NuSTAR is providing 14 an entirely new view of the hard X-ray sky with unprecedented sensitivity. 15 One topic that would benefit from the advent of a LLT is the study 16 of the Type Ia supernovae (SNe Ia). SNe Ia are used as a cosmological

17 standard candle to determine extra-galactic distances, which has led to the 18 astonishing result that the expansion of the Universe is accelerating, implying 19 the existence of dark energy [2, 3]. However, we do not understand why 20 SNe Ia luminosities can be normalized [4], which is related to our lack of 21 understanding of the progenitor system and the physics of the explosion. 22 The spectroscopy and light curve of the line at 847 keV emitted by the decay 23 chain of ⁵⁶Ni, which is massively synthesized in SNe Ia, would discriminate 24 between the currently competing models [5]. A LLT, as featured in the 25 DUAL mission proposal [6], could reach a sensitivity of 2×10^{-6} ph/s/cm² 26 $(3 \sigma, 1 \text{ Ms})$ for a 3% broadened line at 847 keV, enabling detections of a 27 dozen events each year out to ~ 40 Mpc and providing a breakthrough in our 28 understanding of their physics [7]. 29

Another topic is the study of the electron-positron annihilation radiation at 511 keV. This line has been observed for more than 30 years from the Galactic center [8], yet it is still unclear whether known sources can account for all of the 10⁴³ positrons that annihilate every second in the Galactic bulge [9]. New observational clues are needed, requiring both improved sensitivity and angular resolution. A LLT could probe small sky regions to check for structure in the emission and probe some candidate source types, like X-ray binaries.

Other objectives include the study of the emission mechanisms in blazars and active galactic nuclei [e.g. 10] and the physics of stellar mass black holes in binary systems [e.g. 11] through the observation of their emission in energy bands within the 100 keV - 1 MeV domain.

Laue lenses are an emerging technology based on crystal diffraction that 42 enables soft gamma-ray focusing. The advent of this optic would highly ben-43 efit hard X-ray and soft gamma-ray astrophysics, along with other fields. For 44 instance, homeland security and nuclear medicine share the same need for 45 more sensitive gamma-ray detection systems. A Laue lens offers a narrow 46 field of view (typically of $\sim 10'$), and can be designed to focus in a narrow 47 energy bandpass, which can turn into advantages for applications where back-48 ground is an issue and spatial resolution is required (for instance looking for 49 fluorescence lines from a target material, activated by a gamma-ray beam 50 [12]). 51

UC Berkeley's Space Science Laboratory (SSL) joined the effort to de-52 velop Laue lenses in 2010, building upon the experience accumulated over 53 the past 20 years at the IRAP (Toulouse, France) [13, 14, 15]. A dedicated 54 X-ray beamline was completed in Spring 2011, which then allowed the de-55 velopment of an assembly method. The challenge of making a scientifically 56 exploitable Laue lens can be divided in two topics: finding efficient crystals 57 for diffraction, and assembling them accurately enough into a lens. The study 58 and development of crystals for a Laue lens application has been on-going 59 for nearly a decade, resulting in the identification of the best crystals for 60 each energy within the 100 keV - 1 MeV band [16, 17, 18, 19]. The crystal 61 selection is not discussed in this paper. Instead, here we focus on the second 62 aspect, their assembly into a Laue lens. We report on the assembly tools 63 and method that were used to build a breadboard lens made of 15 crystals, 64 and on the calibration procedure and results. This test confirms our ability 65 to reach the crystal orientation accuracy and the packing factor required to 66 build an efficient Laue lens with a focal length of several tens of meters, as 67 required for Type Ia supernovae study for instance [7]. 68

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This paper is organized as follows: The concept of Laue lenses is reviewed

in section 2. Section 3 introduces the coordinate system we used during this
work. Section 4 presents the crystal orientation requirements for a Type Ia
SNe LLT similar to what was presented in Ref. [6], which sets the objectives
for the prototype we assembled. Then we enter the heart of the paper with
the description of the prototype in section 5 and the assembly method in
section 6. The characterization of the lens prototype is presented in section
7, and finally the conclusions are presented in section 8.

77 2. Principle of a Laue lens



Figure 1: Sketch of a Laue lens made of crystals arranged in concentric rings. If the same crystal material and reflection (which determines the d-spacing of the crystalline planes) are used for the two rings of radii r_1 and r_2 , then $E_1 > E_2$, which allows covering a large bandpass. However, if the product of the d-spacing by the radius is constant from ring to ring, the energy diffracted is constant, which allows building up effective area in a narrow energy range.[e.g. 20]

A Laue lens is a concentrator working in the domain of the hard X-rays 78 and soft gamma rays, from ~ 100 keV to ~ 1 MeV. It is based on Bragg 79 diffraction in Laue geometry (*i.e.* the rays go through the crystal) of a large 80 number of crystals arranged such that they all diffract towards a common 81 point on the focal plane (Figure 1) [see e.g. 21, 20, 22]. The crystals can be 82 laid out either in an Archimedean spiral or in concentric rings. The typical 83 cross sectional size of crystals considered for Laue lenses ranges between 4×4 84 mm^2 [23] to $15 \times 15 mm^2$ [24]. 85

In the classical design, each crystal deviates a fraction of the beam without concentrating it. Thus, smaller crystals produce a smaller point spread function (PSF), although at the cost of a larger complexity (larger number to obtain a given collecting area, more difficult to manipulate and orient). Alternatively, a group in Ferrara (Italy) is developing an interesting concept of curved crystals where the diffracted spot of the crystal (hereafter referred to as the crystal's footprint) is smaller than the crystal itself [25].

Perfect crystals are not suitable for Laue lens applications as they behave 93 as monochromators. Even for the case of a Laue lens dedicated to the ob-94 servation of a given nuclear line on the ground¹, crystals with a spread in 95 the orientation of their planes are more efficient than perfect crystals. This 96 is due to the fact that the source is at finite distance, implying that the 97 beam hitting each crystal is diverging. Thus, a crystal can diffract over its 98 full volume only if it presents to the source a bandpass at least matching 99 the angle subtended by its cross-sectional area. Mosaic crystals are the most 100 common mono-crystalline non-perfect crystals. Their bandpass is created 101 by small defects in their crystal lattice². Alternatively, crystals with curved 102 diffracting planes (CDP crystals) can yield higher reflectivity, however they 103 are more difficult to produce [16]. 104

Most Laue lens projects require several thousands of crystals, with focal lengths of several tens of meters. The consequences are twofold: On the one hand, the time devoted to fix each crystal should be as short as possible; and on the other hand, the crystals should be oriented with high accuracy in order to keep the PSF as small as possible. For a given lens design³, the effective area scales with the number of crystals collecting the signal, which is why the crystals should be packed as densely as possible.

¹¹² 3. Lens reference system

Figure 2 shows the reference system we use for this study. The lens plane is XoY, and oZ defines the optical axis, with the rays propagating towards

¹As opposed to an astrophysical context.

²The term *mosaic crystal* comes from the fact that they are well modeled by a juxtaposition of tiny, perfect crystals, slightly disoriented with respect to each other, as proposed by Darwin [26, 27].

³We use the term *lens design* to refer to a given combination of crystals (material, orientation, bandpass), and tile size, and their configuration in the lens (radii, and filling factor of each ring).



Figure 2: *Left:* Lens reference system. See text for details. *Right:* Sketch of four crystals on the lens frame, the fourth being glued.

115 -Z.

The source position $[r_s, \theta_s, \phi_s]$ is defined in spherical coordinates based on the lens reference system. The crystal positions $[r_c, \phi_c, z_c]$ are defined in cylindrical coordinates based on the lens reference system. Each crystal orientation is determined with respect to axes defined by the crystal position on the lens. The orientation is defined by rotations about the radial, tangential, and optical axes, noted $\vec{\theta_R}, \vec{\theta_T}$, and $\vec{\theta_Z}$. In the ideal case and for an on-axis source at infinity, θ_T is the Bragg angle and the two other angles are null.

123 4. Crystal orientation requirements

In order to specify the crystal orientation accuracy requirements, one needs a measure of the impact of crystal angular offset. The only relevant figure is the sensitivity of the telescope. Assuming that the instrumental background is uniform in the focal plane, the sensitivity of the telescope is proportional to the following figure of merit (FoM):

$$FoM = \frac{A_{eff} \epsilon_{PSF}}{\sqrt{A_{PSF}}} \tag{1}$$

where A_{eff} is the lens effective area, and A_{PSF} is the area covered by the fraction ϵ_{PSF} of the PSF (the choice of ϵ_{PSF} is discussed below). This FoM is expressed in cm, but it is more relevant to normalize it by the value obtained for a lens made of ideally oriented crystals.

The distribution of angular misalignment is considered Gaussian and is described by two parameters: its standard deviation, noted $\sigma_{\theta R}$, $\sigma_{\theta T}$, $\sigma_{\theta Z}$, and



Figure 3: Figure of merit (normalized) versus Bragg angle misalignment standard deviation $(\sigma_{\theta T}, \text{left panel})$ and Bragg angle misalignment offset $(\Delta_{\theta T}, \text{right panel})$. In the left panel, the offsets are fixed to 0, and the standard deviation $\sigma_{\theta R}$ and $\sigma_{\theta Z}$ are fixed to 10'. In the right panel, the standard deviations are fixed to 0 and the offsets $\Delta_{\theta R}$ and $\Delta_{\theta Z}$ are fixed to 10'. In both cases, the simulations are done for a 30-m focal length lens made of 10×10 mm² mosaic Ag 111 crystals focusing at 850 keV.

the offset between the center of the distribution and the nominal angle, noted $\Delta_{\theta R}, \Delta_{\theta T}, \Delta_{\theta Z}$, respectively for the 3 angles θ_R, θ_T , and θ_Z . The standard deviation of the distribution affects the width of the energy bandpass and the size of the PSF. The offset of the distribution affects the energy diffracted and the focal length. A crystal ring with a non-zero offset does not focus at the proper focal length, implying a size increase of the PSF.

We decouple the standard deviation from the offset, and we first investi-141 gate the effects of the former. We calculated the FoM for a simulated lens 142 made of 10×10 mm² Ag 111 crystals arranged in a single ring focusing at 850 143 keV with a 30-m focal length. Each crystal has a uniform mosaicity of 45''144 and a mean crystallite size of 100 μm . In these simulations, all the offsets 145 are kept to 0, which means that the mean orientations are nominal along 146 the three axes. Figure 3 shows the FoM as a function of $\sigma_{\theta T}$, the standard 147 deviation of misalignment of the Bragg angle, with both $\sigma_{\theta R}$ and $\sigma_{\theta Z}$ set to 148 10'. For each value of $\sigma_{\theta T}$, the lens' PSF and effective area are simulated and 149 the FoM is derived using the combination of A_{PSF} and ϵ_{PSF} that maximizes 150 it. 151

The FoM is most sensitive to the misalignment of the Bragg angle. One can see in Figure 3 (left panel) that for $\sigma_{\theta R} = \sigma_{\theta Z} = 10'$ and $\sigma_{\theta T} = 0$ the sensitivity loss is merely 2%; however the FoM drops by 10% for $\sigma_{\theta T} = 10''$. One also needs to account for the offset of the distribution along each axis. Another set of simulations was performed. At first, the standard deviations were null, only the offset were varied. This showed that only $\Delta_{\theta T}$ really matters; for $\Delta_{\theta R} = 10'$, $\Delta_{\theta Z} = 10'$ and $\Delta_{\theta T} = 0$, the FoM drops by only 2%, however the FoM drops by 9% if $\Delta_{\theta T} = 10''$ (Figure 3, right panel).

Performing more simulations combining both offset and standard deviation of misalignment for the 3 axes, we derive the orientation requirements in order to limit the FoM loss to 10%. We obtain the following requirements:

 $\sigma_{\theta R} \leq 7'$, $\sigma_{\theta T} \leq 10''$, $\sigma_{\theta Z} \leq 7'$, $\Delta_{\theta R} \leq 5'$, $\Delta_{\theta T} \leq 4''$, $\Delta_{\theta Z} \leq 5'$

¹⁶³ 5. Description of the lens

The prototype lens is composed of 5 Cu crystals and 10 Si crystals ar-164 ranged in 3 sections of concentric rings (Figure 4a), as detailed in Table 165 1. The Cu crystals were produced at the Institut Laue Langevin (Greno-166 ble, France), and the Si crystals were produced at the Institute for Crystal 16 Growth (IKZ, Berlin, Germany). The crystal dimensions are $5 \times 5 \times 3$ mm³ 168 and the crystal interspacing is 0.2 mm at the closest point (distance between 169 the innermost corners of two neighboring crystals). The lens is designed to 170 focus the beam of our X-ray generator (XRG) placed at $r_S = 12.49$ m with 171 a focal length of f = 1.5 m. 172

The crystals are glued on the substrate, thus the orientation relies on the glue bond line. The lens substrate is made of aluminum, with slopes (portions of cones) following the θ_T angle of the crystals in order to keep the glue bond line nearly parallel⁴. The substrate's back side is milled out to reduce passive material, its thickness is about 2 mm. It features holes at the center of each crystal site in order to inject the glue from the back side.

179 6. Assembly method

180 6.1. The Laue lens assembly station

The Laue lens assembly station (LLAS) that we developed at SSL is placed at the end of a 12-m long X-ray beamline using a micro-focus (0.8

 $^{^{4}}$ Crystals are usually cut within 10' of the required orientation, which results in some uncertainty in the bond line shape. This is why we can not rely on the faces of the crystal tiles for the orientation.



Figure 4: a) Laue lens prototype. b) Substrate and crystal towers. The slits defining the beam to $4 \times 4 \text{ mm}^2$ are also visible. c) The beamline at SSL is setup in the high bay. In the foreground is the thermally insulated LLAS. d) Close up on the tip of the crystal holder. The two ledges are visible on the right and side and at the bottom. The red square is a rubber O-ring. e) Full view of the LLAS. The station is setup on a 30×48 inches² Newport table.

Ring	Reflection	Radius	θ_T	Bragg angle	Energy
#	(hkl)	(mm)	(°)	(°)	(keV)
0	Si 111	52.0	0.8734	1.1120	101.878
1	Si 111	57.2	0.9607	1.2231	92.625
2	Cu 111	62.4	1.0479	1.3342	127.565

Table 1: Nominal orientation for each crystal ring of the prototype lens. The difference between the Bragg angle (the incidence angle) and θ_T is due to the fact that the source is at finite distance.



Figure 5: *Left:* autocollimator shot taken with the webcam and processed. The crosshair has been identified as well as the center of the bright green concentric circles, which allows the determination of the angular distance between the center of the circles and the two arms of the cross. *Right:* Evolution of the temperature in the Laue lens assembly station over ten hours.

¹⁸³ mm) XRG operated at 150 kV and 450 μ A (Figure 4c). This beamline was ¹⁸⁴ already presented in Ref. [18] and has not changed since then, however, a ¹⁸⁵ number of changes were implemented in the LLAS (Figure 4e). The LLAS ¹⁸⁶ is composed of the following elements, in the order of the beam propagation:

¹⁸⁷ - A set of slits defining the beam to $4 \times 4 \text{ mm}^2$ (visible in the right hand ¹⁸⁸ side of Figure 4b). The beam position was set prior to the lens assembly ¹⁸⁹ and was not touched after.

- The lens aluminum substrate held by a stack of stages (Figure 4b): a translation perpendicular to the beam (along oY) to change the radius, and a rotation stage (axis oZ) to change the azimuthal position. The rotation axis of this stage defines the axis of symmetry of a ring and thus its optical axis. In addition to these two stages, a manual tilt and rotation stage was inserted on top of the translation stage to orient the substrate with respect to the beam.

¹⁹⁷ - The crystal to be glued, held by the crystal holder (which uses vacuum ¹⁹⁸ suction to maintain the crystal) at the top of a stack of stages allowing ¹⁹⁹ 3-axis rotations. Given our setup (Figure 2), the axes $\vec{\theta_R}$, $\vec{\theta_T}$, $\vec{\theta_Z}$ of ²⁰⁰ the crystal match with the directions -oY, oX, oZ, respectively. The ²⁰¹ stack is mounted on a translation stage (along oZ) to bring the crystal ²⁰² against the substrate once its orientation is correct (Figures 4b and ²⁰³ 4d).

- The detector (visible in Figure 4e). We have been using a planar crossstrip high-purity germanium detector measuring $38 \times 38 \text{ mm}^2$ divided in 19×19 voxels of $2 \times 2 \text{ mm}^2$ [28]. This camera is a prototype for the Nuclear Compton Telescope [29]. It allows the extraction of the spectrum from any number of voxels, with a spectral resolution of 1.3 keV at 122 keV.

In our setup, the crystal being glued is mounted at the tip of the crystal 210 holder, which is centered on the beam. The crystals are glued at $\phi = 270^{\circ}$, 211 diffraction occurring in the horizontal plane (YoZ, see Figurefig:reference). 212 The crystal position and orientation is defined by the plane of the crystal 213 holder, represented as a red square, and by the two ledges of the crystal 214 holder, shown as two red segments in the right panel of Figure 2 (see also 215 Figure 4d). The lens is moved to set the radius r_c and azimuthal angle ϕ_c 216 of the new crystal. The radius r_c is controlled by an oY-translation stage 217 holding the lens, and the azimuthal position of the crystal is controlled by an 218 oZ-rotation stage that holds the lens substrate. One sees in the right panel of 219

Figure 2 that the angles θ_R and θ_T are controlled by the plane of the crystal holder, while θ_Z is controlled by the two ledges of the crystal holder.

In 2011, our first attempt to glue crystals with angular precision lower 222 than 10'' taught us that controlling the temperature is a necessity [18]. The 223 LLAS was thermally insulated and a commercial thermostat coupled to a 224 small fan heater was used to maintain the temperature around 30° C (above 225 the maximum temperature observed in the room). Despite this low-cost 226 system, the temperature was maintained within a range of 1.3° C during the 227 gluing (Figure 5). The big drops in temperature happen when the doors 228 of the LLAS are opened either to setup a new crystal on the holder or to 229 inject the glue. One can see that the total duration for crystal setup and 230 orientation and glue injection was of the order of 30 minutes, followed by 23 about 5 hours of curing time. 232

We use a Davidson Optronics D-656 autocollimator (visible in Figure 4e) 233 with arc-second precision to monitor the orientation of the aluminum sub-234 strate (see section 6.2). We automated the reading of the autocollimator 235 by adding a webcam on the eyepiece and developed software that analyzes 236 the image to return the azimuth and elevation of the bullseye center with 23 respect to the optical axis of the instrument (Figure 5). This was key to the 238 realization of this project as it allows the orientation of the lens substrate to 239 be monitored remotely, without disturbing the temperature. 240

241 6.2. Orienting the substrate

In our setup, the optical axis of a crystal ring is given by the rotation axis of the substrate, which needs to be set for each ring (see below). If this alignment is not done properly, different crystal rings may have different optical axes, leading to an overall PSF increase.

The substrate is correctly oriented when its rotation axis points towards 246 the source. The orientation is set by using the so-called rotating crystal 247 method, involving a crystal⁵ glued at the rotational center of the substrate. 248 The peak energy of the beam diffracted by this crystal is measured for dif-249 ferent azimuthal angles. When the rotation axis points at the source, the 250 peak of the energy diffracted by the crystal is constant for any azimuthal 251 angle. The accuracy of this method was limited in our case to about $\pm 5''$ by 252 the accuracy of the tilt stage (manual tilt and rotation stage Newport 36). 253

⁵We used a perfect Si 111 crystal of $5 \times 5 \text{ mm}^2$ as central crystal.

²⁵⁴ Further details are presented in section 7.4.

Once the initial orientation is done, the substrate is moved to bring the 255 first crystal site in the beam. The autocollimator then becomes the only way 256 to track the orientation of the substrate, as the central crystal is no longer 25 in the beam. Bringing a crystal site in the beam consists in two steps: the 258 substrate is translated along oY to bring the desired radius in the beam (i.e.259 to set r_c), and it is then rotated about oX to bring its rotational axis to 260 point again at the source. The autocollimator is used to measure and correct 261 for the wobble induced by the oY translation stage, and control the rotation 262 about oX as it is done with a manual stage. The autocollimator was also used 263 to monitor the orientation of the substrate while the crystals of a given ring 264 were glued. Despite the poor thermal control, we found that the substrate 265 orientation was very stable with time, so we had to re-orient it only when we 266 were changing r_c . 26

268 6.3. Orienting and gluing crystals

The process to glue a crystal is the following. The crystal is setup at the 269 tip of the holder, the two little ledges defining the angles θ_Z and the plane of 270 the holder defining θ_R and θ_T (Figure 4d). The crystal holder had previously 27 been oriented by using a corner cube and the autocollimator, so its suction 272 plane was perpendicular to the beam and the vertical ledge was vertical (the 273 beam being horizontal). We estimate the error on these angles to be less 274 than 5'. We relied on the crystal external faces for θ_R and θ_Z , which means 275 an orientation accuracy of $\sim 10'$ (based on the cutting specifications). 276

The crystal is first kept 5 mm in front of the face of the substrate for coarse 277 orientation, it is then brought to $\sim 80 \ \mu m$ of the substrate for fine orientation 278 and gluing. The Bragg angle is set using our 0.3'' repeatable oX rotation 279 stage $(\vec{\theta_T})$ to obtain the desired energy diffracted on the camera. When the 280 Gaussian fit of the diffracted peak indicates a misalignment lower than 3'', 28 the glue is injected through the hole in the substrate, using a syringe. The 282 glue, a two-part epoxy (MasterBond EP30-2) meets NASA low outgassing 283 specifications and has a very low shrinkage upon cure, 3×10^{-4} mm/mm. It 284 reaches 85% of its strength after 12h and its ultimate strength is attained 285 after 5–7 days. To speed up the process, the crystal holder was retracted 286 after ~ 5 h of glue curing time. 287

We are currently developing a method to avoid relying on the faces of the crystals for setting θ_Z and θ_R , which would relax the cutting accuracy requirement (thus lowering the cutting cost). The method uses the crystalline

planes perpendicular to $\vec{\theta_T}$ and rocks the crystal about $\vec{\theta_R}$ to diffract in the 291 vertical plane. Finding the diffraction peaks above (1) and under (-1) the 292 horizontal gives the orientation of the crystalline planes and allows adjusting 293 θ_R parallel to the beam. Then the crystal is rotated by $\pi/2$ about θ_T and the 294 same procedure is repeated for $\vec{\theta_Z}$. This method is possible with our setup 295 as the crystal is placed on the rotation axis of θ_T (the bottom rotation stage 296 in picture 4b), which allows a $\pi/2$ rotation while keeping the crystal in the 297 beam. 298

299 7. Characterization of the lens

The characterization was done using full flood illumination (we use a 5mm thick lead mask with an aperture of 2.54×2.54 cm²). The lens substrate is oriented to point at the source and the 15 crystals are centered in the aperture. The beam is strongly diverging in this configuration, but this is fine because the lens was designed for a source at finite distance, at $r_S = 12.49$ m, which is the case here.

The main measurement was performed with the focal plane out of focus, 4 m behind the lens. This allows blowing up the focal point to reveal each individual crystal footprint (Figure 6). This measurement serves two purposes: Firstly, the energy diffracted by each crystal can be measured individually, yielding an accurate measurement of the Bragg angle (θ_T) misalignment. Secondly, the position of the footprint can be used to infer the θ_Z misalignment.

The characterization of the lens was done one month after its assembly, to let enough time for the epoxy to stabilize.

315 7.1. Errors on the Bragg angle

The spectra diffracted by each individual crystal are shown in Figure 7. These peaks are fit with a Gaussian function and the peak energies are converted to angular misalignment using the following formula:

$$\frac{\Delta E}{E} = \frac{\Delta \theta}{\theta} \\ 2d_{hkl}\sin\theta = \frac{hc}{E} \end{cases} \Delta \theta = \frac{\Delta E}{E_{\text{goal}}} \operatorname{arcsin}\left(\frac{hc}{2d_{hkl}E_{\text{goal}}}\right)$$

where the lower equation on the left hand side is the Bragg relation involving the d-spacing d_{hkl} of the crystalline planes (defined by the Miller indices h,



Figure 6: Out-of-focus image acquired with our germanium cross-strip camera. The source is on axis and the detector is placed 4 m behind the lens. The green rectangles are the simulated footprint of the 15 crystals projected onto the detector plane, accounting for orientation errors. One can see that our model of the lens and ray-trace code allow for a good reproduction of the observed pattern.

k and l), θ is the incidence angle of the rays onto the planes, h is Planck's 321 constant and c the speed of light. E_{goal} is the goal energy for a given ring 322 (see Table 1). The resulting angular misalignments are reported in Table 2. 323 Our main goal was to be within the requirements for the Bragg angle 324 standard deviation, $\sigma_{\theta T}$, which is by far the most constraining. While ring 325 0 is far from this goal, rings 1 and 2 are well within it. We showed in Ref. 326 [18] that a standard deviation lower than 6'' is possible with the glue we are 327 using, and we confirm it again with this breadboard lens. The bad figure of 328 ring 0 is likely due to an insufficient curing time. We left the crystal holder in 329 position for only 4.5 h for the first ring, as opposed to 5.0 h to 5.25 h for the 330 two next rings. Another explanation is the high packing factor, combined 331 with the fact that we did not use a glue dispenser. The amount of glue 332 injected was controlled by eye, and most of the time was overflowing on the 333 next crystal's site. We learned as we progressed and improved the procedure 334 for rings 1 and 2. 335

Although the low dispersion in orientation is an excellent result, we see

that the offset of each ring exceeds by far the requirement. Since we glued crystals on small portion of rings, we can not distinguish between an angular offset of the crystals and a misorientation of the substrate. We nonetheless attribute these errors to the substrate orientation; while doing the lens alignment for the calibration measurements, we realized that a problem occurred with the rotating crystal method that led to significant misalignment of the substrate relative to the beam.

This problem is described in detail in section 7.4. As a consequence, the three rings' optical axes are not well co-aligned.

Ring	Cryst. 0	Cryst. 1	Cryst. 2	Cryst. 3	Cryst. 4	$\Delta_{\theta T}$	$\sigma_{\theta T}$
0	52.2 ± 0.5	24.6 ± 0.4	55.0 ± 0.5	77.0 ± 0.5	91.6 ± 0.5	60.1	25.7
1	-13.7 ± 0.5	-6.4 ± 0.4	-12.6 ± 0.4	-13.4 ± 0.4	-22.4 ± 0.4	-13.7	5.7
2	-19.2 ± 0.3	-17.8 ± 0.3	-27.8 ± 0.5	-24.1 ± 0.5	-16.2 ± 0.4	-21.0	4.8

Table 2: Angular misalignment about $\vec{\theta_T}$ in arc-seconds, and associated mean $(\Delta_{\theta T})$ and standard deviation $(\sigma_{\theta T})$ of the distribution.

346 7.2. Errors on the two other angles

After having entered the θ_T misalignments in the lens model, we use the 347 position of the crystal footprints in the out-of-focus image to determine the θ_Z 348 misalignments for each crystal, as reported in Table 3. Our ray trace model 349 indicates that changing θ_Z by 10' leads to a vertical displacement (Y axis in 350 Figure 6) of ~0.5 mm, with no measurable energy change $(5 \times 10^{-5} \text{ keV})$. 351 Our camera has a spatial resolution of 2 mm, which allows us to determine 352 a crystal footprint with a precision of ~ 0.5 mm (interpolating the intensity 353 in each voxel), corresponding to a θ_Z misalignment of ~10'. However, the 354 quantum efficiency cross calibration between strips is estimated to be of the 355 order of 20%. So we did not go through a thorough determination of θ_Z , 356 and simply adjusted it by hand to have the contours of the simulated crystal 357 footprints overlay the measured ones (green rectangles shown in Figure 6). 358

On the other hand, our ray trace model shows that the θ_R misalignment has almost no effect in this configuration; a crystal footprint moves of 70 μ m/degree and the diffracted energy of 0.03 keV/degree. So we can not measure the θ_R misalignment here. Given that the crystals are glued with a bond line of ~80 μ m, we estimate that the error on θ_R can not exceed 27' (40 μ m over 5 mm), and is most likely much smaller than this value. Most crystals have a θ_Z misalignment lower than 10', although the middle crystal of ring 1 is very poorly oriented, with an misalignment of about -4500'' (1.25°). θ_Z was constrained by the two ledges at the tip of the crystal holder, relying on the external faces of the crystals (Figure 4d). A careful mounting of the crystal in the holder seems sufficient to insure a standard deviation of the distribution lower than 10'.

More than a quantitative result, we demonstrate here that it is possible to measure the angular misalignment of crystals using out-of-focus measurement with an imaging camera. An image intensifier with pixels of ~ 0.5 mm, placed 6 m behind the lens, would yield arc-minute resolution.

Ring	Cryst. 0	Cryst. 1	Cryst. 2	Cryst. 3	Cryst. 4
0	-8.3	0	-8.3	-8.3	8.3
1	0	0	-75	-25	0
2	16.7	-25	8.3	-8.3	33.3

Table 3: Crystal misalignment about θ_Z , in arc-minutes. The overlay of the simulated footprints with the measured ones was done by manually adjusting θ_Z for each crystal, by increment of 500" (8.3').

375 7.3. In-focus measurements

For the in-focus measurements, we placed the detector 1.5 m behind the lens. We acquired data with the source close to on-axis ($\theta_S = 12'', \phi_S = 90^\circ$) and 20' off-axis, and compared these data to simulations obtained with the lens model defined earlier.

Figure 8 shows the measured spectra and the simulated contribution of 380 each ring for both source configurations. No background subtraction was 38 performed, and no binning or smoothing was applied. There are two free 382 parameters when fitting the spectrum diffracted by mosaic crystals: the mo-383 saicity and the mean crystallite size (see e.g. [30]). We obtain the best fit with 384 a crystal mosaicity of 8" and 120", and a crystallite size of 1 μ m and 95 μ m 385 for the Si and Cu crystals, respectively. We note that our model (Darwin's 386 model of mosaic crystals [27]) does not reproduce the large wings exhibited 387 by the Cu crystals. This problem is well known and is currently being ad-388 dressed as part of our study of crystals for Laue lenses [16]. Disregarding 380 this point, our ray-trace code and the angular misalignments determined in 390

the previous sections seem to provide a good modeling of the lens spectrum, even for an off-axis angle as large as 20'.

Using the near on-axis run, we measure again the peak energy of each ring (Table 4). Accounting for the fact that the source was 12" off axis, we find angular offsets in agreement with those determined using the out-of-focus acquisition.

Figure 9 shows the images recorded by the detector with the source nearly on-axis and 20' off-axis. The contours of the simulated footprint of the crystals are overlaid in the off-axis case, showing, once again, that we have good agreement between simulation and data. One difference comes from the horizontal streaks produced by the wings of the Cu crystals. In the right panel, one can see the size of the focal spot produced by the 15-crystal prototype lens.

Ring	Goal energy	Measured energy	$\Delta_{\theta T}$
#	(keV)	(keV)	(")
0	101.878	103.177 ± 0.012	63.0 ± 2.5
1	92.625	92.145 ± 0.005	-10.8 ± 2.3
2	127.569	126.776 ± 0.009	-17.8 ± 2.3

Table 4: Goal and measured peak energy for each ring, and derived angular offset (Δ_{thetaT}) .

404 7.4. Analysis of the pointing error

In this section, we analyze the cause of the angular offset between the 405 crystal rings. The substrate was reoriented to point at the source before each 406 ring was populated using the rotating crystal method (section 6.2). While 407 the method is potentially very accurate, our experimental setup introduced a 408 bias. The problem was due to a misalignment between the slits defining the 409 beam and the center of the lens, as illustrated in Figure 10. With a diverging 410 beam featuring a continuum spectrum, the angle of incidence (and therefore 411 the energy diffracted) is position dependent. In Figure 10 (panel a), although 412 the rotation axis points at the source, the peak energy diffracted for the lens 413 azimuthal angle of 180° is shifted towards low energy with respect to the 414 peak energy diffracted at 0° . This would appear as if the rotation axis was 415 not pointing at the source. One can see in Figure 10 (panel b) that the key 416 point is to have the lens' center aligned with the center of the slits. 417



Figure 7: Diffracted spectrum extracted for each crystal from the out-of-focus image (Figure 6). No background subtraction was performed, and no smoothing or binning was applied.



Figure 8: Diffracted spectrum measured at the focus with the source nearly on-axis (left), and 20' off-axis (right). The simulated contribution of rings 0, 1 and 2 (green, blue and red lines, respectively) are shown as well.



Figure 9: Images acquired with the camera placed at the focus of the lens with the source nearly on-axis (left), and 20' off-axis (right). The simulated footprints of the 15 crystals comprising the lens are shown in the right panel. The horizontal streaks are due to the wings of the Cu crystals.



Figure 10: Illustration of the artifact that occurred with the rotating crystal method. The crystal is represented by the grey rectangle, the dashed lines symbolizing the diffracting planes. In both a) and b) cases, the crystal is shown at two azimuthal angles of the lens, 180° apart, the dash-dot line representing the rotation axis. The colors used in the diffracted beam represent the energy, from low (red) to high (blue) energy.

In the present case, the substrate positioning was done by eye (thanks 418 to a laser that goes through the beamline and shows the beam) with an 419 estimated precision of ~ 1 mm, which results in an offset of the rotation axis 420 of order of 16.5". This explains the offset observed for rings 1 and 2. For 421 ring 0, our conclusion is that a mistake was made when the substrate was 422 shifted from the rotating crystal position (center of the lens in the beam) to 423 the gluing position (ring 0 in the beam) and then rotated to face the beam, 424 which was done with a manual rotation-and-tilt stage. 425

It is clear from that experience that the orientation of the lens substrate is as sensitive as the orientation of the crystals themselves. The lens substrate should be mounted on a three-axis motorized stack of stages with a repeatability of the order of 1", and a better system should be used for monitoring the orientation of the substrate.

431 8. Conclusions

For more than two years a Laue lens assembly process has been under development at the Space Sciences Laboratory. It required the construction of an X-ray beamline and a dedicated end station, the so-called Laue lens
assembly station. These tools and methods were tested with the realization of
a breadboard Laue lens made of 10 silicon crystals and 5 copper crystals glued
onto an aluminum substrate. Our goal is to meet the stringent requirements
on crystal orientation accuracy imposed by the long focal length (30 m)
necessary to build a LLT dedicated to the study of Type Ia supernovae.

The results of this first trial are very encouraging: considering ring 0 440 a trial run, we were able to quickly refine the assembly process and meet 441 the requirement of 10" standard deviation on the Bragg angle misalignment 442 for ring 1 and 2. The packing factor is as high as possible, with a nominal 443 interspacing of 0.2 mm. However, the lens reference system showed its limits 444 resulting in a poor co-alignment of each ring's optical axis. Although there 445 are improvements to be made, this prototype shows that the criteria for 446 building an efficient LLT for Type Ia SNe are within our reach. 44

The realization of a prototype also demonstrated our ability to simulate a Laue lens for the case of a source at finite distance, which is key to the assembly and calibration of any lens. Indeed, even a lens designed for sources at infinity would be assembled and calibrated in a diverging beam. A calibration procedure was developed and successfully applied to the characterization of the lens.

The realization of this prototype served its purpose: test the tools and 454 methods, and identify the critical points for further refinement. The LLAS 455 is currently being upgraded in preparation for a second prototype assembly. 456 The emphasis is on improving the thermal stability of the enclosure and the 457 control of the substrate orientation with respect to the X-ray beam. We are 458 also investigating alternative glues allowing the curing time to be significantly 459 reduced. The next prototype will be composed of crystals optimized for 460 diffraction at 120 keV, and the calibration procedure will have to determine 461 the reflectivity in addition to the angular misalignments. We intend to put 462 this next prototype through thermal-vacuum cycles and vibration tests, in 463 order to move the Laue lens technology closer to technology readiness level 6, 464 which would then allow it to be proposed for balloon-borne or satellite-borne 465 missions. 466

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