# Sensor Measurement Strategies for Monitoring Offshore Wind and Wave Energy Devices

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## 5 Abstract

6 While the potential of offshore wind and wave energy devices is well 7 established in terms of environmental impact, operations and maintenance 8 issues are still not very well researched or understood. One of the important 9 aspects in this regard is the lack of access to these devices since they are 10 typically situated in high wind and wave conditions to generate more energy. 11 Consequently, deployment of sensors for such devices is an important issue 12 since they can measure the response of these devices in an as-deployed 13 condition and assessments or intervention decisions may be made based on 14 the fusion of data of such sensors and through the choice of intelligent 15 markers or modelling. While scaled model testing of devices in ocean basin 16 has gained popularity and wide acceptance over time, research in the 17 direction of developing guidelines for sensor measurement or placement 18 strategies are currently not in place. This paper addresses some specific 19 aspects of sensor choice, measurement and placement. In this regard, the 20 performances of the sensors are considered in terms of their receiver 21 operating characteristics (ROC) and uncertainties related to measurements are 22 addressed. The option of using multiple, cheaper sensors of seemingly 23 inferior performance as opposed to the deployment of a small number of

24	expensive and accurate sensors is also explored. Practical aspects of testing
25	are addressed in terms of exposure conditions and the performance of
26	different sensors. Tests have been carried out in an ocean wave basin and the
27	sensor placement for these tests has been used as a case study.

## 28 **1 Introduction**

29 Both offshore wind and wave energy technology has seen major advances in 30 recent years. Wave energy in particular is growing in popularity (Falcão 31 2010; Mccullen et al. 2002). Operations and maintenance (O&M) costs are a 32 highly relevant factor in the overall financial assessment of such projects, all 33 the more so in offshore projects due to lower availability of the device 34 (O'Connor et al. 2013). This has pushed the need for reliable structural 35 monitoring systems for accurate and reliable information about the health of 36 these energy conversion devices. With a move in recent times towards 37 offshore energy solutions, loss in ease of accessibility may lead to damage 38 going undetected, and the increased risk of catastrophic failure (Swartz et al. 39 2010).

There is clear financial benefit to optimizing time between inspections and scheduled maintenance work, which affects the uptime of systems while also coming with their own costs- an unscheduled maintenance event is five times more costly than one that is scheduled (Adams et al. 2011). However, high costs related to some sensing systems outweigh the benefits to O&M cost savings so the value of expensive sensing systems must be evaluated.

There are many forms of sensing systems, based on various technologies.
Accelerometers have been successfully applied to identifying and locating the
presence of structural damage in offshore structures (Mangal 2001), as well
as motion cameras and load cells (V.JAKSIC; ref; ref) and Fiber Bragg

50 Grating (FBG) to measure strain. Cameras can even be employed in 51 underwater situations to detect damage (O'Byrne et al. 2014) where marine 52 growth exasperates fatigue damage. However, little is known of the relative 53 merits of these technologies.

54 Wireless sensor networks (WSN) are a promising technology which have in 55 recent years gained much attention from academia and industry alike. The 56 application of WSN technology to structural health monitoring (SHM) has 57 the potential to provide a substantial and quantifiable improvement to 58 existing monitoring solutions for civil infrastructure (Boyle et al. 2011) 59 .While wired SHM systems would require more maintenance and more frequent site visits as wires can be damaged over time, wireless SHM systems 60 61 offer flexibility, even on difficult to access structures, and significantly 62 reduced costs of installation and maintenance.

However, some of the existing wireless systems for SHM still have high
power consumption. The high power consumption and the limited power
budget make these systems unsuitable for long-term installation on a structure
and requires frequent site visits for system maintenance.

WSN nodes are battery powered and because of their limited energy source
they are not suitable for long-term structural health monitoring applications.
With the focus on enhancing the life time of a wireless sensor node, a popular
is by complementing an energy harvesting technique with an efficient energy
management algorithm (Sharma et al. 2010). This approach has the potential

to achieve self-sustainability of the node with harvesting energy from the
environment and effectively managing the node activity (i.e. the sampling
rate of the sensors) according to the energy levels and the dynamics of the
phenomenon observed (Srbinovski et al. 2015unpublished)

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# 77 2 Experimental Model

# 78 **2.1 Model**

A scaled Tension Leg Platform (TLP), a truss like structure with a hexagonal
base, was tested in this study. This device consists of a gravity base
connected by six mooring tethers to the Buoyancy Ring and the Upper
Structure and the Tower and Nacelle, all as shown in fig 1.



Figure 1 TLP Model

## 85 **2.2 Instrumentation and Testing**

The model was instrumented with 6 Tedea-Huntleigh stainless steel single 86 ended bending beam load cells which were attached to the six mooring line 87 88 cables and bolted to the gravity base. These measured the cable tension in 89 Newtons (N). The instantaneous positions of 3 reflective markers, which 90 were attached to the six corners of the hexagonal base, were monitored by 4 91 Qualisys 3-Series Oqus Marker Tracking Cameras with a sampling frequency 92 of 32Hz. A Laser Doppler Vibrometer (LDV) was also employed during 93 testing to record the velocity of the TLP. This high resolution technology 94 samples at a rate of 480 Hz. Displacements and velocities were recoded in the 95 wave direction, as this was considered the most critical plane.

96 The model was tested at the Hydraulics and Maritime Research Centre
97 (HMRC), University College Cork (UCC), Ireland in its Ocean Wave Basin.
98 A variety of periods and wave amplitudes were used and the Bret Schneider
99 wave spectrum was chosen, to best represent a true sea state.

# 101 **3 Results**

# 102 **Displacement**

The camera recorded the position of the TLP at 3 different locations; the
Inner Ring, the Outer Ring and the Middle Mast. The velocity of the structure
as recorded by the LDV was used to find displacement values.

Figure 2(a) shows the displacements recorded by the camera at the 3 tracked positions. Due to the far larger amplitude of displacement at the mid mast position, due to the flexible nature of the mast and its sensitivity, these readings were omitted from the average value shown in figure 2 (c), as they were viewed to be skewing the data (see figure 2 (b) ).





2(a)

**2(b)** 



**2(c)** 

112 Figure 2 Displacment

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# 115 Velocity

116 The LDV records velocity, and the displacement data recoded by the camera

117 is used to derive its velocity. In figure 3, the RMS values of velocity for each

118 test are shown for both the motion camera and the LDV.



121 Figure 3 RMS Velocity of Camera and LDV data

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123 Values recorded for the LDV are increasingly higher than those derived from 124 the camera for each successive test of increased wave period. The camera's 125 data here is inaccurate in that it doesn't increase proportionally with the 126 increase wave loading.

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# 128 Frequency

The displacement time series for the LDV and the motion camera were
converted into the frequency domain with a Fourier Fast Transform (FFT).
The dominant input to the series, the waves acting are the dominant

#### frequency in this output, seen as the largest peaks (Figure 4).





Figure 4 Fourier Fast Transform of Camera Displacement Time Series

By comparing analysis outputs to known inputs for two different technologies, we can compare the retained accuracy of each. In Figure 4, the response of frequency of the output for the two different instruement is compared to the known frequency of the wave input to the system. The peak frequency of the velocity output of the LDV is, on average, 18.7% lower than the wave frequency of each particular test. Whereas the peak frequency of the camera's displacement is an average of 31.9% higher than the same inputs.



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Figure 5 Frequency comparison of input wave to frequency of LDV and camera displacement outputs

- 150 The same comparison, but for the frequency of the LDV's velocity output
- 151 yielding a difference of only 7%, on average, from the wave input.

# 152 Load Cells

- 153 Load cells were placed at Bow Port, Bow Starboard, Mid Starboard, Stern
- 154 Starboard, Stern Port, Mid Port and were accordingly labelled White, Red,
- 155 Yellow, Green, Brown and Blue.
- 156 The average Peak and RMS load values for each load cell for 20 different
- 157 tests are represented in Figure 6. The highest loads are recorded in the
- 158 direction of the wave, at the bow and at the stern of the structure. Analysis of
- the effect of removing different load cells to the overall data was carried out,
- a sample of which is shown in Figure 7.









Data obtained from the white cell at Bow Port was removed, and the estimate
shown for loading at this position shows a loss in accuracy of the loading on
the structure.

# 4 Energy Aware Adaptive Sampling Algorithm for EnergyHarvesting WSNs

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171 The development of WSNs technology is hindered by their limited energy 172 supply. In the case of SHM applications, sensors are extremely expensive 173 with respect to energy requirements. It is desirable to develop protocols that 174 effectively manage the sensor power consumption while still meeting the 175 requirements of the application. Adaptive sampling algorithms (ASA) are 176 often used as a tool to minimize the communication between the sensor nodes 177 within the network and at the same time to minimize the power consumed by 178 the sensors by reducing the sampling rate according to the needs of the 179 phenomenon observed.

An ASA presented in (Alippi et al., 2010) was implemented in Matlab and
evaluated using data collected with sensor for DISPLACEMENT as recorded
by the motion cameras.

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The algorithm used evaluates the maximum frequency of the signal using FFT and then decides the sampling frequency by multiplying the maximum frequency with a constant which is  $\geq 2$  satisfying the Nyquist criterion. A 187 detailed description of the implemented algorithm with all relevant188 parameters explained can be found in (Alippi et al., 2010).



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190 Figure 8 Matlab ASA Implementation of Camera Displacement Data

191 In figure 8, the sampling frequency according to the ASA and the maximum 192 frequency of the signal are presented. The graph was generated by 193 implementing ASA in Matlab with the following values for the relevant parameters: c = 2.1, h = 5, W = 50,  $\delta$  = 0.1%. Details for each of these 194 195 parameters are explicitly given in (Alippi et al., 2010). The time between successive frames was 0.3125, thus the starting sampling frequency was 196 197 32Hz. As shown in figure X, using the ASA reduces the number of acquired 198 samples with respect to the traditional fixed sampling rate approach and 199 hence saves energy.

# 201 9 Discussions and Conclusions

202 A comparison was made between high quality LDV data and lower quality 203 motion camera data which recorded 3 different locations on the structure. It 204 was initially thought that the multiple positions being tracked would increase 205 accuracy, but due to physical characterists of the mid mast location, the extra 206 data was misleading of the overall structure and reduced overall accuracy of 207 results. Fewer, better placed markers which took into account physical set up 208 of model would have been more effective. However, for the load cells, a 209 higher number of locations monitored leads to a better understanding of the 210 structure under wave loading.

211 Section 4 deals with the optimisation the number of acquired samples to save 212 energy. In applications where a battery powered system is used to interface a 213 power hungry sensor, reducing the sampling rate when possible will extend 214 the life of the battery while still maintaining the application data 215 requirements. Dynamically changing the sampling frequency according to the 216 needs of the phenomenon under observation can also improve the data 217 quality. Using fixed sampling rate can cause undersampling of the signal, 218 hence introducing error in the measurement and difficulties in reconstructing 219 the signal and this method helps to avoid this.

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